

STORMWATER MANAGEMENT REPORT

FOR

GALILEEE EGLISE ADVENTISTE INCORPORATED PROPOSED CHURCH

BLOCK 3301, LOT 4 NEPTUNE TOWNSHIP

MONMOUTH COUNTY, NEW JERSEY

PREPARED BY:

B&G ENGINEERING LLC. 30 BERNARD DRIVE EWING, NEW JERSEY 08628

November 29, 2022

BESRICK G. PLUMMER, P.E. NEW JERSEY PROFESSIONAL ENGINEER LICENSE NO. 39534

B&G PROJECT NO. 1943A

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INTRODUCTION

The scope of this report is to discuss the storm-water management measures proposed for the planned improvements at the subject site located in Neptune Township, Monmouth County, New Jersey, (see Figure 1- Project Location Map). The proposed storm-water management system has been designed in accordance with the New Jersey Department of Environmental Protection and Neptune Township Stormwater Management Standards, per New Jersey Administrative Code Section 7:8-5.5. Storm-water routing calculations in this report are in accordance with USDA Soil Conservation Service Technical Release No. 55 (TR-55), "Urban Hydrology for Small Watersheds".

Storm	24-hour depth (inches)
2-year	3.49
10-year	5.40
100-year	9.24

PROJECT DESCRIPTION

The proposed project involves the construction of a one (1)-story house of worship with basement at the project site. The proposed building footprint will be 80 ft x 50 ft and it will be constructed on the west side of the existing one (1) story single-family residence currently on site. The church sanctuary will be physically connected to the existing house (garage section), and the existing house will be converted to religious office spaces and ancillary uses.

To facilitate the proposed improvements some existing onsite infrastructure will be demolished including existing asphalt driveways, concrete walkways and other miscellaneous site features. In addition, several trees and shrubs will be removed to allow for construction of proposed site features required to serve the needs of the church.

Site improvements include the construction of a 64-space parking lot including three (3) handicap accessible parking spaces, installation of concrete curb and sidewalk, and construction of a 14' x 14' trash enclosure. An infiltration basin has been proposed to meet the storm-water management requirements of the NJDEP, Freehold Soil Conservation District and Neptune Township. This basin will be located north of the proposed sanctuary and behind the existing dwelling. A pre-formed scour hole is proposed downstream of the infiltration basin to account for emergency overflow from the infiltration basin. The proposed storm system discharging to the infiltration basin will consists primarily of reinforced concrete culvert pipes (15"-24") and associated drainage inlets. Roof leaders from the church building will connect to HDPE and PVC pipes. These pipes will tie into the main storm sewer system.

Onsite open space areas will consist of parking lot and site landscaping per Neptune Township landscaping requirements. Several shade trees, shrubs, along with ground cover and perennial

grass are proposed throughout the site. Since the site is heavily wooded, the on-site landscaping will be supplemented by existing trees and shrubs that will remain.

Existing onsite utilities that will remain and serve the proposed church include a 4-inch sanitary lateral that connects to an existing sanitary main on State Highway 33, and a domestic water well to provide potable water use.

SITE DESCRIPTION

The site is located on the northern side of New Jersey State Highway Route No. 33 between West Bangs Ave to the west and Fairview Ave in the east, in Neptune Township, Monmouth County, New Jersey, (See Figure 1, Appendix "A"). A review of the official tax map of the Township identifies the site as Lot 4, Block 3301. Its postal address is 3313 NJ 33, Neptune, NJ 07753

Presently the site is occupied by a one (1) story single-family residence with an attached one-car garage, and a wooden deck. In addition to the residence, other onsite structures include a one-story frame building, a wooden shed and a wooden gazebo. Vehicular access to the site is via an existing paved driveway from NJ Route 33.

The site is almost rectangular in shape and is heavily wooded along all property lines. To the north the site is bordered by Shark River Brook, aka Jumping Brook which flows southwards and is a tributary to Shark River. To the south the site is bordered by NJ Route 33 (Corlies Ave), and commercial buildings. West of the site is a single-family residence and wooded areas, while east of the site is a United Methodist Church and wooded areas.

On site utilities include a 4-inch sanitary lateral, a domestic water well, and electric and gas services. Open space includes several shade and flowering trees, shrubs and lawn areas.

A review of the existing topography within the area of proposed disturbance shows a relatively flat site with slopes of from 1.0% to 5% (area of major site and building improvements.). The exception to the mild slopes is in the area of the proposed infiltration basin and pre-formed scour hole, where the average slope is over 30%.

Pre-development stormwater runoff at the site generally flows from four (4) drainage areas in a sheet flow like pattern across and from the site, to adjacent properties to the west and to Route 33 to the south. To the north and east stormwater flows to Shark River Brook, a tributary of Shark River. There is no existing onsite storm sewer system to convey stormwater runoff, resulting in areas of standing water at low lying paved areas during heavy rainfalls. The existing onsite soil is sandy with a favorable infiltration rate allowing water from pervious areas to seep through the soil.

In the areas associated with the proposed sanctuary, and parking lot construction, the existing ground cover is mostly pervious, except for areas of existing onsite driveway and approximately 2,000 SF of parking area. Therefore, stormwater runoff is minimal due to the existing sandy soils. Rainfall infiltrates the soil after various storm events and there is little evidence of onsite erosion due to the porous soils.

SOIL CHARACTERISTICS

A review of the United States Department of Agriculture/Soil Conservation Service Soil Survey of Monmouth County New Jersey, indicates that there are two (2) soils series at the project site. A closer review shows that within the proposed area of disturbance, the onsite soil is Lakehurst Sand (LakB), occurring on 0% to 5% slopes, (See Figure 2- Project Soils Map, Appendix "B"). In addition, at the rear of the site, outside of the proposed limit of disturbance, the other soil series is Humaquepts, (HumAt), occurring on 0 to 3 percent slopes.

The Lakewood soil series is described as having a depth to restrictive feature of more than 80 inches and is a moderately well drained soil. Onsite soil tests revealed an infiltration rate of 4.5 inches/hour in the area of the proposed infiltration basin.

Its typical soil profile is 0 to 2 inches of slightly decomposed material, and 2 to 80 inches of sand. Its hydrologic soil group is "A" based on its high infiltration rate. Appendix "B" of this report gives a detailed description of the soil series. The Onsite Soil Exploration Report is also included in Appendix "B".

The following sections detail the calculation methodologies and results of the storm-water management design.

PRE-DEVELOPMENT DRAINAGE CONDITIONS

The proposed stormwater management for this project has been designed to meet NJDEP storm water management requirements for "major development". Presently there are no designed stormwater management structures at the subject site. However non-structural features such as lawn areas provide TSS removal for stormwater runoff. In addition, the existing onsite soil is sandy in nature which allows for stormwater recharge.

The existing drainage areas are shown on the Pre-development Drainage Area Map in Appendix "E. A review of this map shows four (4) distinct drainage areas all flowing offsite un-detained. The area consists of parking lot and driveway (CN = 98) and pervious areas (CN = 39 for grass and CN = 30 for woods). The resulting storm-water rates and volumes generated for the pre-development conditions (see Appendix "C" & Pre-Development Drainage Area Map, Appendix "G"), is shown in the table on the next page.

	DA #1	DA #2	DA #3	DA #4
Area (SF)	7247	39472	37279	5931
Curve Number	39	47	44	47
Time of Concentration (min)	6.5	7.2	9.1	6.6
2 Year Rate (cfs)	0.00	0.02	0.01	0.00
25 Year Rate (cfs)	0.01	0.40	0.21	0.06
100 Year -Rate (cfs)	0.26	2.51	1.83	0.39

POST-DEVELOPMENT DRAINAGE CONDITIONS

The proposed stormwater management for this project has been designed to meet NJDEP storm water management requirements for "major development". The project involves the construction of a one (1)-story house of worship with basement at the project site. The proposed building footprint will be 80 ft x 50 ft and it will be constructed on the west side of the existing one (1) story single-family residence currently on site. The church sanctuary will be physically connected to the existing house (garage section), and the existing house will be converted to religious office spaces and ancillary uses.

Site improvements include the construction of a 64-space parking lot including three (3) handicap accessible parking spaces, installation of concrete curb and sidewalk, and construction of a 14' x 14' trash enclosure. An infiltration basin has been proposed to meet the storm-water management requirements of the NJDEP, Freehold Soil Conservation District and Neptune Township. This basin will be located north of the proposed sanctuary and behind the existing dwelling. A pre-formed scour hole is proposed downstream of the infiltration basin to account for emergency overflow from the infiltration basin. The proposed storm system discharging to the infiltration basin will consists primarily of reinforced concrete culvert pipes (15"-24") and associated drainage inlets. Roof leaders from the church building will connect to HDPE and PVC pipes. These pipes will tie into the main storm sewer system.

The proposed drainage areas to the infiltration basin is shown on the Post -development Drainage Area Map in Appendix "G. This area is modeled as fourteen subcatchment areas, both detained and undetained, due to site topography and ground cover. The area consists of parking lot and driveway (CN = 98) and pervious areas (CN = 39 for grass and CN = 30 for woods). The resulting storm-water rates and volumes generated for the post development conditions is included in Appendix "C" of this report and can be summarized as follows:

	DA #1	DA #2	DA #3	DA #4	DA #5	DA #6	DA #7
Area (SF)	5194	10842	3636	11746	5947	1843	5726
Curve Number	64	72	81	54	54	39	82
Time of Concentration (min)	6	6	6	6	6	6	6
2 Year Rate (cfs)	0.08	0.38	0.20	0.04	0.02	0.00	0.33
25 Year Rate (cfs)	0.25	0.89	0.40	0.35	0.18	0.00	0.65
100 Year -Rate (cfs)	0.67	2.06	0.81	1.33	0.68	0.08	1.29

	DA #8	DA #9	DA #10	DA #11	DA #12	DA #13	DA #4a
Area (SF)	4165	6623	4405	9263	3590	4473	4351
Curve Number	87	88	86	81	78	89	39
Time of Concentration (min)	6	6	6	6	6	6	6
2 Year Rate (cfs)		0.49	0.30	0.52	0.17	0.34	0.00
25 Year Rate (cfs)	0.53	0.86	0.55	1.02	0.36	0.59	0.01
100 Year -Rate (cfs)	0.99	1.59	1.04	2.05	0.76	1.08	0.16

PROPOSED STORMWATER MANAGEMENT DESIGN

The proposed storm-water management design consists of the construction of one (1) storm-water management infiltration basin providing 22,933 cf. of storage at elevation 43.73ft, and a preformed scour hole acting as a stable downstream discharge point.

The infiltration basin will control storm-water runoff generated by the reconstructed and new parking lot, driveways, and other site improvements. This storage is provided between elevations 38.0 and 45.00, with the 100- year water surface elevation at 43.73 ft. An emergency spillway is provided at elevation 45.00, to a preformed scour hole, located downstream of the basin.

All frequency storms up to and including the 100 yr storm will flow to the infiltration basin. A proposed onsite storm sewer system will convey storms including the 25 yr frequency storm to the infiltration basin, via open channel flow.

The resulting storm-water improvements will provide pre-treatment and reduce the rate and volume of storm-water runoff flowing from the project area.

STORMWATER COMPLIANCE

The proposed improvements will result in 1.86 acres of disturbance and a net increase of 0.81 acre of impervious coverage. This project falls under NJDEP's definition of a "major development". NJDEP requirements for groundwater recharge, water quality and low reductions are being achieved by the proposed infiltration basin. The infiltration basin will provide 80% TSS removal to the developed area, meeting the NJDEP water quality requirements.

The Flow and Volume reduction requirements are summarized below.

Flow Comp

POA	Exist	Target	Proposed	Delta
2	0.02	0.01	0.10	+0.09*
10	0.62	0.46	0.37	-0.11
100	4.92	3.93	1.30	-2.63

^{*}See below Volume Table

Volume Comp

POA	Exist	Prop	Delta	
2	0.015	0.011	-0.004	
10	0.101	0.034	-0.067	
100	0.402	0.108	-0.294	

Time for basin to drain

For 100-year storm:

Peak Basin Elevation = 43.73 ft @ 17.80 hours

Basin at Invert Elevation 38.00 @ 53.10 hours

Basin drains in 35.3 hours

The basin infiltration rates are based on in-situ soils testing. The infiltration rate was measured at 4.5-inches per hour, See Appendix "C". A design rate of 2.25-inches per hour was used, in accordance with NJDEP Best Management Practices. This infiltration rate is in keeping with the USDA Soil designation of Lakehurst Sand, HSG A.

PRIMARY SPILLWAY ROUTING (ASSUMING FULL BASIN)

The emergency spillway consists of an outlet structure with a grate at elevation 44.50. The structure discharges to an 18-inch pipe ending at a scour-hole at elevation 42.00. Assuming that the basin is in failure, with no exfiltration and the water surface at 44.50, a 100- year storm will reach a maximum elevation of 44.80, with a velocity into the scour hole of approximately 6.0 feet per second. The scour-hole as designed will attenuate this velocity and prevent downhill soil erosion.

SOIL EROSION & SEDIMENT CONTROL

Soil Erosion and sediment control measures are proposed for this project based on Freehold Soil Conservation District Soil Erosion & sediment Control Standards. Silt fence and storm drain inlet protections are specified to be installed at designated locations as shown on sheet 9 of the Site Plan documents. A stabilized construction access (min length 50 ft) is shown at the proposed access point for construction activities. The Freehold Soil Conservation District Standard General Notes are included on Sheets 9 & 10 of the Site Plan documents, along with construction details and notes.

ON SITE STORM SEWER COMPUTATIONS

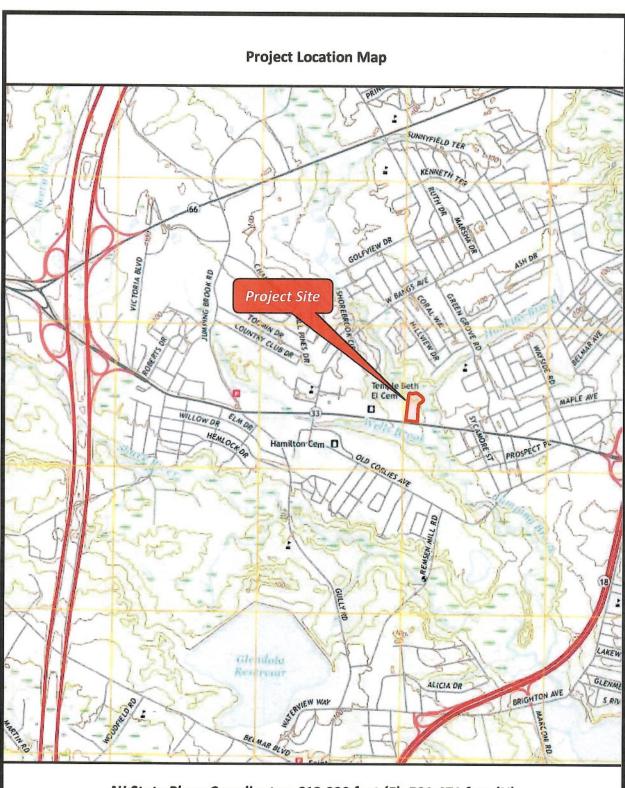
Storm sewer capacity calculations were done using Manning's Equation for open channel flow. An "n" value of 0.013 was utilized for reinforced concrete pipe. A tabular layout of the storm sewer calculation is included in Appendix "E". The calculations in Appendix "E" show that the proposed on-site storm sewer system has the design capacity to convey the 25-year storm runoff for the proposed improvements.

CONCLUSIONS

The proposed infiltration basin has been designed to address the NJDEP stormwater management requirements. All flow reductions requirements and TSS removal will be addressed with the planned improvements. The onsite storm sewer system is designed to convey the 25 yr frequency storm as discussed herein and as shown in the calculations included in appendix "E" of this report.

APPENDIX A

FIGURE 1 – PROJECT LOCATION MAP



NJ State Plane Coordinates: 612,020 feet (E), 501,471 feet (N)

Map Source: USGS 7.5-Minute Series, Asbury Park, NJ Quadrangle (2019)

APPENDIX B

SOILS MAP, SOILS DESCRIPTION & SOIL INVESTIGATION REPORT

Soils Map



Legend

HumAt – Humaquepts, 0 to 3 percent slopes, frequently flooded LakB – Lakehurst sand, 0 to 5 percent slopes

Map Source: USDA NRCS Web Soil Survey (2020)

Monmouth County, New Jersey

LakB—Lakehurst sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 4j88

Elevation: 20 to 150 feet

Mean annual precipitation: 28 to 59 inches
Mean annual air temperature: 46 to 79 degrees F

Frost-free period: 161 to 231 days

Farmland classification: Not prime farmland

Map Unit Composition

Lakehurst and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Lakehurst

Setting

Landform: Dunes, flats

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Parent material: Sandy fluviomarine deposits

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 4 inches: sand E - 4 to 18 inches: sand Bh - 18 to 32 inches: sand BC - 32 to 45 inches: sand C - 45 to 54 inches: sand Cg - 54 to 80 inches: sand

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): High to

very high (2.00 to 19.98 in/hr)

Depth to water table: About 18 to 42 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Quakerbridge

Percent of map unit: 5 percent

Landform: Knolls, flats

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex, linear Across-slope shape: Linear Hydric soil rating: No

Atsion, rarely flooded

Percent of map unit: 5 percent Landform: Flats, depressions

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, dip, talf

Down-slope shape: Linear, concave Across-slope shape: Linear, concave

Hydric soil rating: Yes

Berryland, rarely flooded

Percent of map unit: 5 percent

Landform: Flats, depressions, drainageways
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope

Down-slope shape: Linear, concave Across-slope shape: Linear, concave

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Monmouth County, New Jersey

Survey Area Data: Version 14, Jun 1, 2020

Monmouth County, New Jersey

HumAt—Humaquepts, 0 to 3 percent slopes, frequently flooded

Map Unit Setting

National map unit symbol: 1j1jd

Elevation: 0 to 300 feet

Mean annual precipitation: 28 to 59 inches
Mean annual air temperature: 46 to 79 degrees F

Frost-free period: 161 to 231 days

Farmland classification: Not prime farmland

Map Unit Composition

Humaquepts, frequently flooded, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Humaquepts, Frequently Flooded

Setting

Landform: Flood plains
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Loamy alluvium

Typical profile

A - 0 to 18 inches: loam C - 18 to 60 inches: sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 6.00 in/hr)

Depth to water table: About 0 to 12 inches Frequency of flooding: FrequentNone Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Moderate (about 7.2

inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: A/D Hydric soil rating: Yes

Minor Components

Manahawkin, frequently flooded

Percent of map unit: 5 percent Landform: Flood plains Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Mullica, occasionally flooded

Percent of map unit: 5 percent

Landform: Flood plains, depressions, drainageways Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear, concave Across-slope shape: Linear, concave

Hydric soil rating: Yes

Atsion

Percent of map unit: 5 percent

Landform: Flats

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Dip, talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Monmouth County, New Jersey Survey Area Data: Version 16, Aug 30, 2022



CONSULTANTS, INC. 4405 South Clinton Avenue South Plainfield, NJ 07080

Tel: (800) 545-ATUL (908) 754-8383 Fax: (908) 754-8633

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March 08, 2021

B & G Engineering LLC 30 Bernard Dr Ewing, NJ 08628

Attn:

Mr. Besrick Plummer

President

Re:

Subsurface Soil Investigation Report

Proposed Infiltration Basin 3313 Corlies Avenue Township of Neptune Monmouth County, NJ Block # 3301, Lot # 4

Dear Mr. Plummer.

Enclosed, please find three (3) copies of the the Subsurface Soil Investigation and Foundation Recommendation report for two (2) soil borings and one (1) field percolation test performed on February 17, 2021 at the project referenced above.

Soil samples collected during the subsurface soil investigation program will be discarded after thirty (30) days from the date of this report, if not requested in advance to do otherwise. We thank you very much for providing us an opportunity to service you on this project.

Should you have any question or require additional information, please do not hesitate to contact the undersigned at (908)754-8383.

Sincerely.

ANS Consultants, Inc.

Atulkumar N. Shah, PE

President

New Jersey PE License # 24GE03443900

ANS/RM

Copy to: B & G Engineering LLC- (3), file- (1)

File: ANX-5349_01.SB

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Fax: (908) 754-8633

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March 08, 2021

B & G Engineering LLC 30 Bernard Dr Ewing, NJ 08628

Attn:

Mr. Besrick Plummer

President

Re:

Subsurface Soil Investigation Report

Proposed Infiltration Basin 3313 Corlies Avenue Township of Neptune Monmouth County, NJ Block # 3301, Lot # 4

Dear Mr. Plummer.

Enclosed, please find three (3) copies of the Subsurface Soil Investigation and Foundation Recommendation report for two (2) soil borings and one (1) field percolation test performed on February 17, 2021 at the project referenced above. The work was performed as per our signed proposal dated February 11, 2021.

Our Scope of Services included the following:

- Drilling and full-time inspection of two (2) soil borings down to maximum 17'-0" depth or to refusal, whichever comes first, including recording of groundwater level and also seasonal high-water table if encountered.
- 2. Perform field percolation test in one of the soil boring location.
- 3. Preparation of a written report summarizing all findings and recommendations.

PROPOSED MONSTRUCTIONS

The project site is located at 3313 Corlies Avenue, Township of Neptune, NJ in Monmouth County. At present, the subject site consists of a 1½ story dwelling. We understand that the borings and field percolation test were conducted for the proposed infiltration storm drain system at the subject site. The soil borings and the field percolation test were performed towards rear of the subject property. Please see soil boring & percolation test location plan in Appendix-A and photographs in Appendix-C for more details.

SITE CONDITIONS:

The subject site is located towards north side of Corlies Avenue. Primarily the subject site is located in residential & commercial surroundings. At the time of soil boring work, the site was noted to be fairly leveled. The subject site is located at latitude of N 40° 12' 34.93" and Longitude of W 74° 04' 13.97". As per the DeLorme Topo Quad Map the subject site is at the elevation of 37 feet above mean sea level. Please, see site location plan in Appendix-A and Photographs in Appendix-C for more details.

FIELD INVESTIGATIONS:

SOIL BORING:

Soil Boring locations were marked by the ANS field representative as per the proposed location Plan provided by the client and based upon the equipment access. Sub-Surface utility mark-out was performed by New Jersey-One call System. Once, cleared the soil boring work began on February 17, 2021.

Two (2) soil borings, B-1 and B-2 were drilled during the geo-technical investigation at the site on February 17, 2021. Both the borings were performed at the location shown in Soil Boring & Field Percolation Location Plan included in Appendix-A. The soil boring work was performed under the direction and supervision of our field Engineer Mr. Syed Abbas. Drilling work was performed using an Acker Track Rig XLS with hollow stem auger. As per the drawing provided by the client, the ground contour elevation was noted to be 44.50' which is the starting elevation for the borings. Soil samples were collected continuously down to 18 feet depth in boring B-1 and down to 20 feet depth in boring B-2. Soil samples were extracted using a 2" diameter split spoon sampler as the sampling procedure specified in ASTM 1586-99.

Samples were obtained by the Standard Penetration Test (SPT) Method (ASTM D 1586), which consists of driving a 2-inch outside-diameter split-spoon sampler into the soil with a 140-pound weight falling freely through a distance of 30 inches. The sampler was driven in four successive 6-inch increments, with the number of blows per increment being recorded. The number of blows required to advance the sampler the middle 12 inches is termed the Standard Penetration Resistance (N-value) and is presented on the Field Test Boring Logs in Appendix-A.

During drilling operations, extracted soil samples were visually examined and classified by our Field Engineer. The soil sample description, Standard Penetration Resistance Test (SPT) blow counts and locations, strata changes, groundwater depth and other pertinent information were recorded on a detailed field log. Soil samples obtained at the SPT locations were visually classified according to the Unified Soil Classification System (USCS). Samples were later returned to our laboratory for further review and testing.

FIELD PERCOLATION TEST:

One (1) field percolation test was performed on February 17, 2021 at a location shown on the attached location plan. Test was performed by drilling a hole at location using augurs to test depth and installing a 2" diameter PVC pipe. Bottom of pipe was secured at test depth and pipe was filled to top with water. Ground at test depth was saturated for 2 hours by refilling PVC pipe again and again whenever its level dropped down from top. After 2 hours of saturation, refilling of pipe was ceased and drop in water level was recorded for every 15 minutes interval.

- Depth of test: 7'- 6" below existing ground elevation.
- 2. Water was filled to top of PVC pipe at 1:16p.
- 3. Two (2) hours saturation time ended at 3:16p.
- Water was levelled off to top of pipe at 3:16p and drops in water level at 15 minutes interval were recorded.

Sr. No.	Time	Drop in Water Level	Remarks	Percolation Rate per Hour
1.	3:16 pm	Water was filled to top of PVC pipe.		

2.	3:31 pm	1 1/4"	Ti Ti	
-		1 %		5"
3.	3:31 pm		Refilled	
4.	3:46 pm	1 1/4"		5''
5.	3:46 pm	W	Refilled	
6.	4:01 pm	1 1/8"		4 1/2"
7.	4:01 pm		Refilled	*
8.	4:16 pm	1 1/8"		4 1/2"
9.	4:16 pm		Refilled	
10,	4:31 pm	1 1 <i>/</i> 8"		4 1/2"
11.	4:31 pm		Refilled	
12.	4:46 pm	1 1/16"		4 1/4"
13.	4:46 pm		Refilled	And the second of the second o
14.	5:01 pm	1 1/16"		4 1/4"
15.			Refilled	The second secon
16.	5:16 pm	1 1/16"		4 1/4"
			A STATE OF THE PARTY OF THE PAR	No. 645 (57)

Average Percolation per Hour = 2x5" +3 x 4 1/2"+ 3x4 1/4"

8 = 36 1/4"

8 = 4.53125"

LABORATORY TESTING:

Two (2) soil samples, one each from borings B-1 and B-2 were laboratory tested to determine in-place moisture content and to classify the soil as per Unified Soil Classification System ASTM-D2487-93. The test results are summarized below and a complete Laboratory test results are included in Appendix-B.

Soil Boring No.	Soil Sample No.	Depth collected	Moisture Content (%)	Fines thru #200 Sieve	USCS Symbol
B-1	S-1	4' - 6'	10.2	18.2	SM
B-2	S-2	2'-4'	7.6	8.3	SP-SM

SM: Silty Sands SP-SM: A mixture of Poorly Graded sands and Silty Sands

SUBSURFACE CONDITIONS:

A detailed description of the soil encountered during soil boring activities is documented in the summary table below. The following gives a general description of the subsurface conditions encountered. While the sampled area may indicate that the subsurface conditions appeared to be relatively uniform across the site, it should be recognized that the size of the sampled area was quite small compared to the size of the site, and that the existence of anomalies cannot be precluded.

According to NJ Geoweb website, the geological formation is upper stream terrace deposits and geologic age is middle to late Pleistocene. It consists of sand and pebble gravel, minor silt and cobble gravel; yellow, reddish yellow, yellowish brown. As much as 20 feet thick.

Based on the results of soil borings and our geo-technical laboratory testing, we estimate the general stratigraphy of the site to consist of the following major units, in an increasing order of depth.

Stratum 1: Fill material containing gray-black and grayish brown/black silt, trace fine gravel, trace fine roots & grayish brown silty fine sand, trace f/c gravel, some fragments of concrete, trace fragments of wood & dark gray-black/yellowish-orange f/c sand, trace silt, some f/c gravel, yellowish-orange clay/dark gray orange clayey silt was noted in top 8' in boring B-1 and down to 16' in boring B-2.

Stratum 2: Very dark gray-black silt, trace f/m sand, trace fine gravel was noted between 10' to 12' in only boring B-1.

<u>Stratum 3:</u> Gray-dark gray & orange clayey silt/dark gray clay trace fine sand, trace f/c gravel was noted between 12 feet to 18 feet in only boring B-1.

Stratum 4: Very dark gray sandy silt, trace coarse gravel and dark gray f/c sand and fine gravel, trace silt, trace fragments of clay was noted was noted between 18' to 20' depth in only boring B-2.

SUMMARY OF FINDINGS:

Boring Number	Depth in (feet)	Penetration Resistance, N-Value	Soil Type	In-Place Soil Bearing Capacity (PSF)	Recommended Safe Soil Bearing Capacity (PSF)
B-1	0-2	12	FILL	2400	1500
B-1	2-4	6	FILL	1200	1500
B-1	4-6	7	FILL	1400	1500
B-1	6-8	31	FILL	+5000	1500
B-1	8-10	11	FILL	2200	1500
B-1	10 –12	2	SM-ML	400	1000
B-1	12 –14	. 5	CL-ML	1000	1000
B-1	14 16	5	CL-ML	1000	1000
B-1	16-18	8	CL	1600	1500

Boring Number	Depth in (feet)	Penetration Resistance N-Value	Soil Type	In-Place Soil Bearing Capacity (PSF)	Recommended Safe Soil Bearing Capacity (PSF)
B-2	0-2	16	FILL	3200	2000
B-2	2-4	9	FILL	1800	2000
B-2	4-6	25	FILL	5000	2000
B-2	6-8	16	FILL	3200	2000
B-2	8-10	10	FILL	2000	2000
B-2	10 -12	20	FILL	4000	2000
B-2	12 -14	16	FILL	3200	2000
B-2	14 16	19	FILL	3800	2000
B-2	16-18	5	No	1000	1000
B-2	18 -20	10	SP-SM	2000	2000

GROUNDWATER:

Groundwater was encountered at 9'-4" in boring B-1 (at elevation +34.00') and at 9'-9" in boring B-2 (at elevation +34.25') below existing grade surface. It should be noted that groundwater level will fluctuate due to variations in rainfall or other factors not evident at the time of our investigation.

SEASONAL HIGH WATER TABLE:

Due to fill material noted in both borings, mottling or Seasonal High water table was not noted in both borings.

CONCLUSIONS & RECOMMENDATIONS:

- 10 Groundwater was encountered at 9'-4" in boring B-1 and at 9'-9" in boring B-2 below existing grade surface. Consequently, we anticipate that groundwater management during construction will be critical if any excavation for utility will be placed below this level.
- Fill was noted in top 8' in B-1 and down to 16' in B-2. The majority of on-site soil consisted of clayey-silt/clay with trace fine sand & f/c gravel in boring B-1 and sandy silt with trace coarse gravel in boring B-2. On site soil will be unsuitable as structural fill. Depending upon the time of the year when the actual construction takes place, drying of excavated soil and aeration may be required to reduce the moisture content. In-situ moisture content of soil varied in between 7.6 % to 10.2 % which is generally considered moist.
- The safe soil bearing capacity in top 8 feet was noted between 1,500 PSF to 2,000 PSF in B-1 3. and B-2. We recommend utilizing 1,500 lbs/sq.ft in-place soil bearing capacity to design any footings for the structures.
- 4. Field percolation rate was noted to be 4.53125 inch/hr.
- 5. All fill material shall be placed in lifts on the order of twelve (12) inches in loose thickness and be uniformly compacted to at least 95% of its maximum dry density as determined by the modified proctor density values derived based upon ASTM D-1557-93 test procedure. In addition, we recommend that backfill soils placed in confined areas, such as foundation or utility excavations, to be spread in lifts on the order of six to eight inches in loose thickness and be compacted to the same degree using manually operated vibratory compaction equipment.

Soil Unit weight (total):

110 pcf

Angle of Internal Friction:

28 degrees

Coefficient of sliding friction:

0.4

Coefficient of active earth pressure: 0.28

Coefficient of passive earth pressure: 3.57

RECOMMENDED SERVICES:

It is recommended that we should be retained to provide continuous observation and Soil Engineering services during the excavation and foundation construction phases of the work. This is to observe compliance with the design concepts, specifications and recommendations, and to allow design changes in the event that subsurface conditions differ from those anticipated prior to start of construction.

LIMITATIONS:

The recommendations contained in this report are our best professional judgment as to be

followed in the design and construction of the proposed project based on the subsurface information, plans and criteria referred to in this report. There may be subsurface conditions not disclosed by the explorations adequately identify subsurface conditions for the purpose of this study. If changes in location or character of this project are subsequently amended or if, during construction any differences are found between the report of the explorations and the actual subsurface conditions, they should be brought to our attention immediately so that the effect on our recommendations can be evaluated.

This report has been prepared in accordance with generally accepted Geotechnical Engineering practices for the exclusive use of B & G Engineering LLC and their designated representative (s). No other warranty, express or implied is made. Contractor's wishes to use the soil boring information may do at their own risk. Unless specifically indicated to the contrary in this report, this report does not address environmental considerations, which may affect the site development. The conclusions and recommendations of this report are not intended to supersede or overlook any NJDEP and Federal Environmental rules and regulations, which should be reflected in the site planning.

Should you have any questions or require additional information, please, do not hesitate to contact the undersigned at (908)754-8383.

Sincerely,

ANS Consultants, Inc.

Atulkumar N. Shah, PE

President

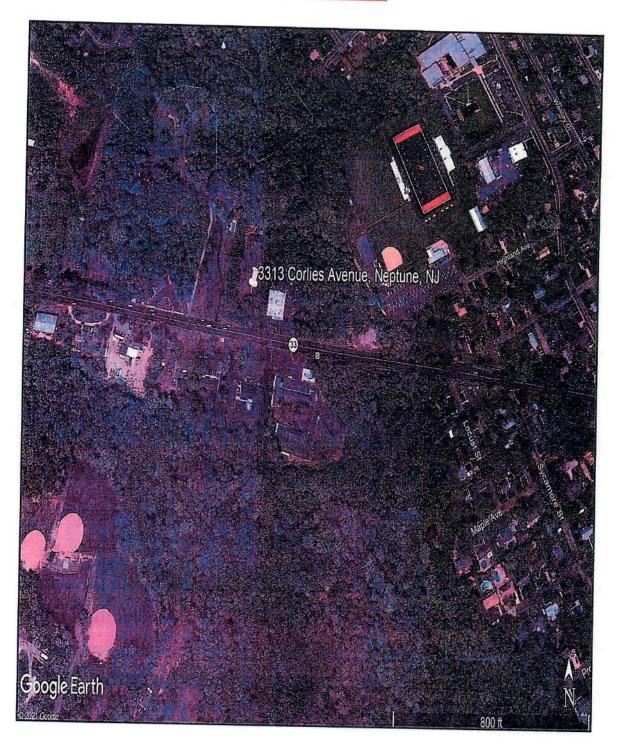
New Jersey PE License # 24GE03443900

ANS / RM

Copy to: B & G Engineering LLC- (3), file- (1)

Appendix-A

GOOGLE MAP

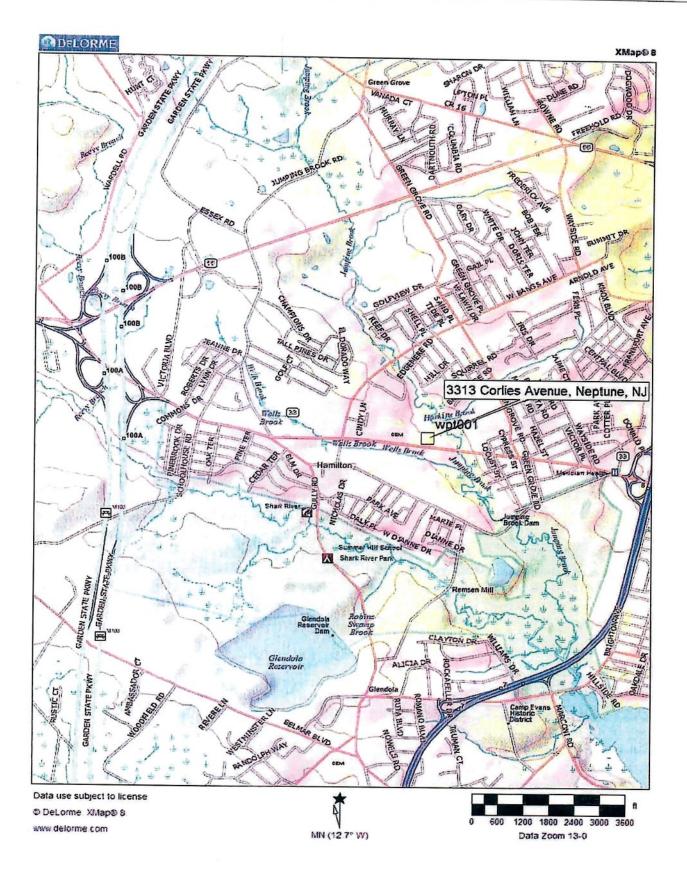


Client: B & G Engineering, LLC Project: 3313 Corlies Avenue

Twp of Neptune, Monmouth County NJ

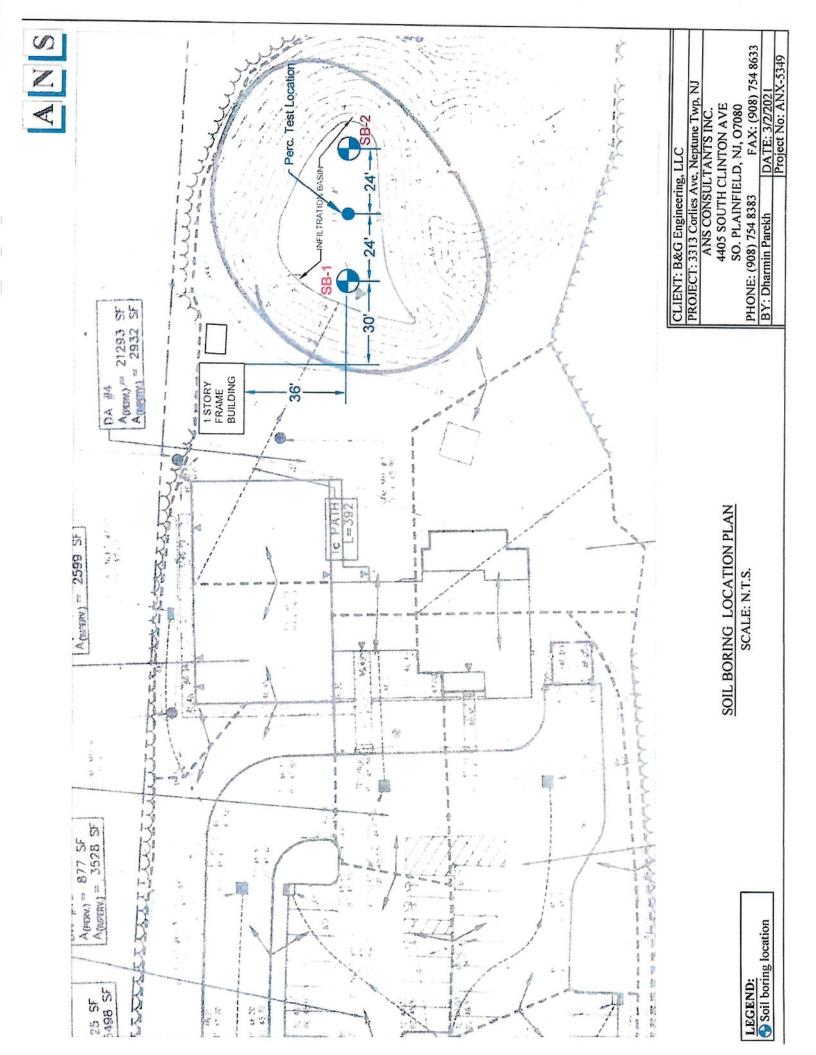


CONSULTANTS, INC. 4405 South Clinton Avenue South Plainfield, NJ 07080



SITE LOCATION MAP 3313 Corlies Ave, Twp of Neptune, NJ





Project: 3313 Corlies Avenue, Neptune, NJ

Report of Testpit / Soil Boring

TP -1 /B-1

S. No.	Depth	N-Value	Recovery	Description of Soil
1.	0 - 2'	12	20"	Fill: 1. Top soil: 1" 2. Top 12": Gray black and grayish brown silt, trace fine gavel, trace fine roots, moist. 3. Bottom 7": Grayish brown silty fine sand, trace f/m gravel, moist.
2.	2' - 4'	6	5"	Fill: Dark gray silty fine sand, trace f/c gravel, moist.
3.	4' - 6'	7	10"	Fill: Dark gray and grayish brown silty fine sand, trace fine gravel, moist.
4.	6' - 8'	31	9"	Fill: Dark gray and grayish brown silty fine sand, trace fine gravel, some fragments of concrete, trace fragments of wood, moist.
5.	8' - 10'	11	11"	Fill: Dark gray silty fine sand and fragments of concrete, trace fine gravel, moist.
6.	10' - 12'	2	6"	Virgin Soil: Very dark gray-black silt, trace f/m sand, trace fine gravel, wet.
7.	12' - 14'	5	11"	Gray-dark gray and orange clayey silt, trace fine sand, trace fine gravel, wet.
8.	14' - 16'	5	24"	Gray-dark gray and yellowish orange clayey silt, trace f/c gravel, wet.
9.	16' - 18'	8	10"	Dark gray clay, moist.

Ground water @ 9'-4"

Project: 3313 Corlies Avenue, Neptune, NJ

TP -2 /B-2

S. No.	Depth	N-Value	Recovery	Description of Soil
1.	0 - 2'	16	20"	Fill: Dark gray-black silt, trace fine sand, trace f/c gravel, trace roots, trace fragments of concrete (bottom of spoon), moist.
2.	2' - 4'	9	7"	Fill: Dark gray-black f/c sand, trace silt, some f/c gravel, moist.
3.	4' - 6'	25	10"	Fill: Yellowish-orange clay and fragments of concrete, some silt, some f/m gravel, moist.
4.	6' - 8'	16	13"	Fill: Dark gray-orange clayey silt, some fragments of concrete, some f/m gravel, s/wet.
5.	8' - 10'	10	10"	Fill: Gray f/c sand and fine gravel, trace silt, some fragments of concrete, s/moist.
6.	10' - 12'	20	12"	Fill: Gray-black and yellowish-orange f/c sand, trace silt, some fine gravel, some fragments of concrete, s/moist.
7.	12' - 14'	16	11"	Fill Top 8": Dark gray f/c sand, trace silt, some f/c gravel, trace fragments of concrete, wet. Fill Bottom 3": Grayish orange f/c sand and fine gravel, trace silt, wet.
8.	14' - 16'	19	17"	Fill: Top 11": Black and orange f/c sand, trace silt, some f/m gravel, trace fragments of concrete, wet. Fill Bottom 6": Black and brown fragments of wood, wet.
9.	16' - 18'	5	NR	
10.	18' - 20'	10	21"	Virgin Soil top 13": Very dark gray sandy silt, trace coarse gravel, wet. Bottom 8": Dark gray f/c sand and fine gravel, trace silt, trace fragments of clay, wet.

Ground water @ 9'-9"

Project: 3313 Corlies Avenue, Neptune, NJ

Report of Field Percolation Test

One field percolation test was performed at a location shown on attached location plan. Test was performed by drilling a hole at location using augurs to test depth and installing a 2" diameter PVC pipe. Bottom of pipe was secured at test depth and pipe was filled to top with water. Ground at test depth was saturated for 2 hours by refilling PVC pipe again and again whenever its level dropped down from top. After 2 hours of saturation, refilling of pipe was ceased and drop in water level was recorded for every 15 minutes interval.

- 1. Depth of perc test: 7"-6" below existing ground elevation.
- 2. Water was filled to top of PVC pipe at 1:16 pm.
- 3. Two (2) hours saturation time ended at 3:16 pm.
- 4. Water was levelled off top of pipe at 3:16 pm and drops in water level at 15 minutes interval were recorded.

S. No.	Time	Drop in Water Level	Remarks	Percolation Rate Per Hour
1.	3:16 pm	Water was fille PVC p	ed to top of ipe	
2.	3:31 pm	1 1⁄4"		5"
3.	3:31 pm		Refilled	
4.	3:46 pm	1 1⁄4"		5"
5.	3:46 pm		Refilled	
6.	4:01 pm	1 1/8"		4 1/2"
7.	4:01 pm		Refilled	
8.	4:16 pm	1 1/8"		4 1/2"
9.	4:16 pm		Refilled	
10.	4:31 pm	1 1/8"		4 1/2"
11.	4:31 pm		Refilled	
12.	4:46 pm	1 1/16"		4 1/4"
13.	4:46 pm		Refilled	
14.	5:01 pm	1 1/16"		4 1⁄4"
15.			Refilled	

Project: 3313 Corlies Avenue, Neptune, NJ

16.	5:16 pm	1 1/16"	4 1/4"

Average Percolation Rate Per Hour =
$$\frac{2 \times 5" + 3 \times 4\frac{1}{2}" + 3 \times 4\frac{1}{4}"}{8}$$
$$36\frac{1}{4}"$$

FIELD SOIL CLASSIFICATION SYSTEM

PARTICLE SIZE IDENTIFICATION

COHESIONLESS SOIL

(Gravel, Sand, Silt and Combinations)

Boulders8 inch diameter or greater Cobbles3 to 8 inch diameter Gravel Coarse 1 to 3 inch
Medium 1/2 to 1 inch
Fine 4.75 mm to 1/2 inch
Sand Coarse 2.0 mm to 4.75 mm
(dia. of pencil lead)
Medium 0.425 mm to 2.0 mm
(dia. of broom straw)
Fine 0.075 mm to 0.425 mm
(dia. of human hair)
Silt & Clay Smaller than 0.075 mm

DENSITY

Very Loose 05	blows I ft or less
Loose06	to 10 blows / ft
Medium Dense11	to 30 blows / ft
Dense 31	to 50 blows / ft
Very Dense51	

COHESIVE SOIL

(Clay Silt and Combinations)

RELATIVE PORTIONS

Descriptive Term	Percent
Trace - tr	1 - 10
Some - sm	
Adjective - ly	21 - 35
And - &	36 - 50

CONSISTENCY

Very Soft	01 blow / ft or less
Soft	02 to 4 blows / ft
	05 to 8 blows / ft
	09 to 15 blows / ft
	16 to 30 blows / ft
	31 blows / ft or greater

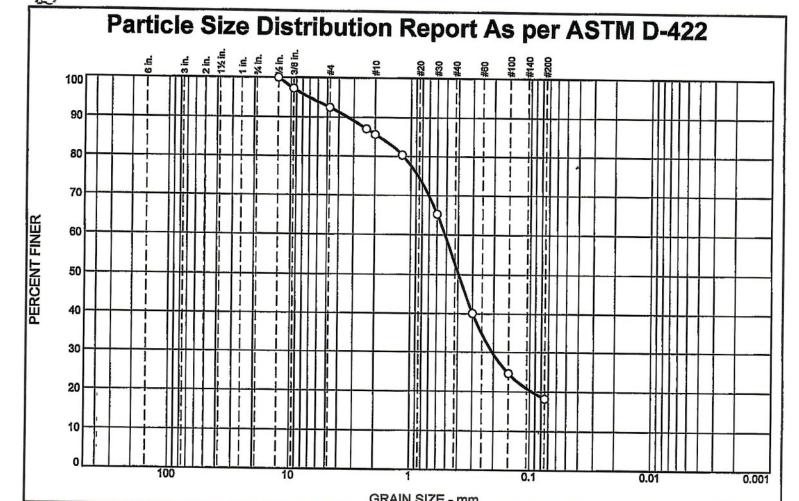
ARRDEVIATIONS

ABBREVIATION	S
Bn - Brown	_
Gy - Gray	
Blk - Black	
Rd - Red	
Or - Orange	
BI - Blue	
Lt - Light	Coarse grained - c
Dk - Dark	Medium grained - i
Multi - Multi colored	Fine grained- f

ROCK

R.Q.D.	Rock Quality
00 - 25	Very Poor
25 - 50%	
50 - 75%	.Fair
75 - 90%	Good
90 - 100%	

HSA - Hollow Stem Auger SS- Split Spoon Sampler WOR - Weight of Rods WOH - Weight of Hammer NR - No Recovery of Sample Appendix-B



% +3"	% Gr			% Sand		% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	7.6	6.7	32.9	34.6	18.2	

SIEVE	PERCENT	SPEC.*	PASS?
SIZE	FINER	PERCENT	(X=NO)
1/2 3/8 #4 #8 #10 #16 #30 #50 #100 #200	100.0 97.3 92.4 87.1 85.7 80.4 65.2 40.1 24.6 18.2		

Brown in color. s	Material Description ilty sand	<u>on</u>			
PL= NP	Atterberg Limits LL= NV	PI= NP			
D ₉₀ = 3.3740 D ₅₀ = 0.3953 D ₁₀ =	Coefficients D ₈₅ = 1.8519 D ₃₀ = 0.2049 C _u =	D ₆₀ = 0.5156 D ₁₅ = C _c =			
USCS= SM	Classification AASHT	O= A-2-4(0)			
Remarks Sample was collected on 02/17/21 and tested on 02/25/21. In-Situ %MC=10.2 F.M.=2.13					

Location: B-1, 4'-6' Sample Number: S-1

Depth: 4'-6'

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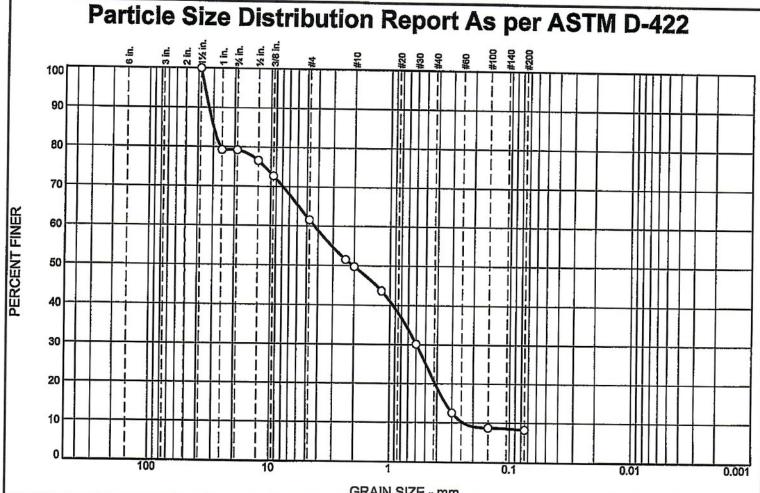
Project: 3313 Corlies Avenue, Township of Neptune, Block # 3301, Lot # 4

South Plainfield, New Jersey

Project No: ANX-5349

Figure 1 F 1

Date: 02/25/2021



GRAIN SIZE - IIIII.							
% +3"	% Gr	% Gravel		% Sand		% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	20.7	17.7	11.9	29.1	12.3	8.3	
			The second second				

SIEVE	PERCENT	SPEC.*	PASS?
SIZE	FINER	PERCENT	(X=NO)
1.5	100,0		
1	79.3		
3/4	79.3		
1/2	76.6		
3/8	72.8		
#4	61.6		
#8	51.5		
#10	49.7		
#16	43.6		
#30	30.2		
#50	12.5		
#100	8.7		
#200	8.3		
	500000000000000000000000000000000000000		

(no specification provided)

Location: B-2, 2'-4' Sample Number: S-2

Depth: 2'-4'

Material Description

Dark brown in color, poorly graded sand with silt and gravel

Atterberg Limits
LL= NV PL= NP PI= NP Coefficients D₉₀= 32.6536 D₅₀= 2.0533 D₁₀= 0.2429 D₈₅= 29.8317 D₃₀= 0.5964 C_u= 17.68 $\begin{array}{c} D_{60} = 4,2933 \\ D_{15} = 0.3408 \\ C_{c} = 0.34 \end{array}$ Classification USCS= SP-SM AASHTO= A-1-a Remarks Sample was collected on 02/17/21 and tested o 02/25/21. In-Situ

%MC=7.6

F.M.=4.40

Date: 02/25/2021

ANS CONSULTANTS, INC.

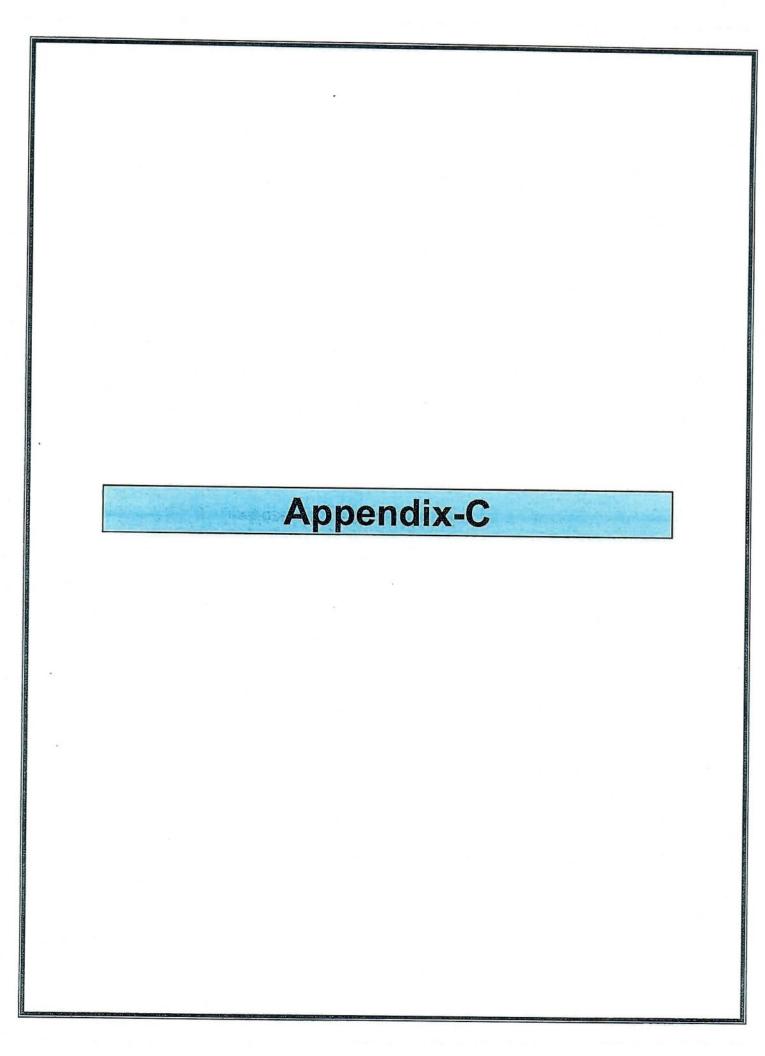
Client: B&G Engineering LLC

Project: 3313 Corlies Avenue, Township of Neptune, Block # 3301, Lot # 4

South Plainfield, New Jersey

Project No: ANX-5349

Figure 2 F 1





Project: 3313 Corlies Ave, Twp of Neptune, NJ



Sample procurement using split spoon samplers and augurs



Sample recovery from split spoon samplers



Project: 3313 Corlies Ave, Twp of Neptune, NJ



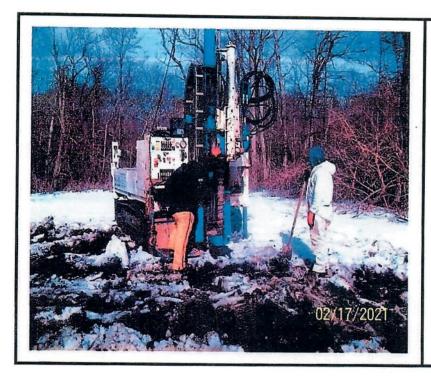
Sample recovery from split spoon samplers



Sample recovery from split spoon samplers



Project: 3313 Corlies Ave, Twp of Neptune, NJ



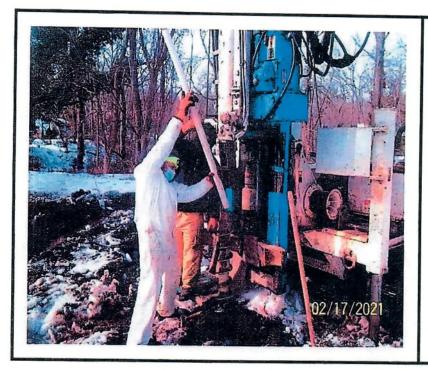
Sample procurement using split spoon samplers and augurs



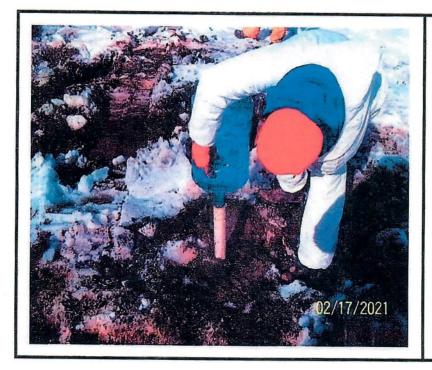
Sample procurement using split spoon samplers and augurs



Project: 3313 Corlies Ave, Twp of Neptune, NJ



Sample procurement using split spoon samplers and augurs



Field Percolation Test



Project: 3313 Corlies Ave, Twp of Neptune, NJ



Sample procurement using split spoon samplers and augurs



Sample recovery from split spoon samplers

APPENDIX E

PRIMARY SPILLWAY ROUTING CALCULATIONS (ASSUMING FULL BASIN)

1943A-Proposed 20221024 no exfiltration

Prepared by {enter your company name here}

HydroCAD® 10.10-3a s/n 03590 © 2020 HydroCAD Software Solutions LLC

Page 1

Summary for Pond 1P: INFILTRATION BASIN

[80] Warning: Exceeded Pond 13P by 5.26' @ 17.44 hrs (23.47 cfs 8.734 af)

Inflow Area = 1.480 ac, 63.46% Impervious, Inflow Depth = 6.35" for 100-Year event

Inflow 12.86 cfs @ 12.00 hrs, Volume= 0.783 af

Outflow = 10.56 cfs @ 12.04 hrs, Volume= 0.783 af, Atten= 18%, Lag= 2.1 min

Primary 10.56 cfs @ 12.04 hrs, Volume= 0.783 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs. dt= 0.01 hrs.

Starting Elev= 44.50' Surf.Area= 4,001 sf Storage= 26,003 cf

Peak Elev= 44.80' @ 12.04 hrs Surf.Area= 4,001 sf Storage= 27,206 cf (1,203 cf above start)

Plug-Flow detention time= 435.6 min calculated for 0.186 af (24% of inflow)

Avail Storage Storage Description

Center-of-Mass det. time= 1.7 min (794.3 - 792.6)

Invert

Volume

volume	1110	eri Avall.Sto	rage Storage	Description	
#1	38.0	00' 28,0	04 cf Custom	Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
38.0 45.0		4,000 4,001	0 28,004	0 28,004	
Device	Routing	Invert	Outlet Devices	s	
#1	Device 2	2 44.50		oriz. Orifice/Gra	te X 12.00 columns X 12 rows C= 0.600
#2	Primary	42.50'	Inlet / Outlet In	o, square edge h	neadwall, Ke= 0.500 2.00' S= 0.0500 '/' Cc= 0.900

Primary OutFlow Max=10.55 cfs @ 12.04 hrs HW=44.80' TW=0.00' (Dynamic Tailwater)

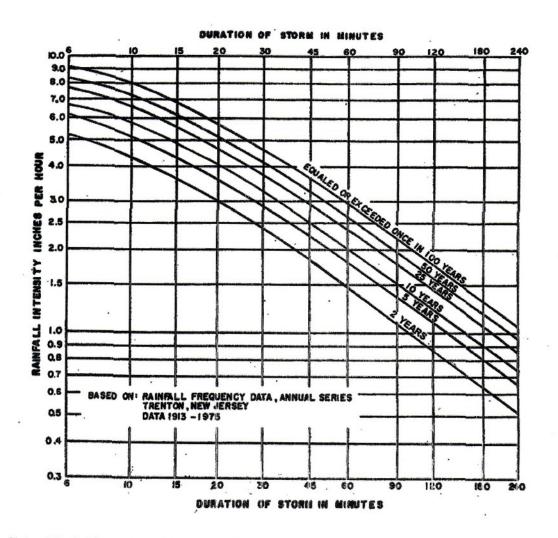
2=Culvert (Passes 10.55 cfs of 10.59 cfs potential flow)

1=Orifice/Grate (Orifice Controls 10.55 cfs @ 2.64 fps)

APPENDIX F

NJDEP IDF CURVES
ON-SITE STORM SEWER COMPUTATIONS
CONDUIT OUTLET PROTECTION
CALCULATIONS
PREFORMED SCOUR HOLE CALCULATIONS
HYDROLOGIC MODELING DATABASE DATA
ENTRY FORM

FIGURE 7.2 RAINFALL INTENSITY CURVES



Note: Adapted from Figure 2.1-2 in the NJDEP Technical Manual for Stream Encroachment Permits.

B		# E-3		# B-5		# B-4		# E-2		# A-2		RD		#A-3		#E-1		# B-3		# B-2		# B-1	LOC)	П		TOWNSHIP	PROJ
	MH# 1		#E-3		# B-5		# B-5		# E-2		#A-2		# A-2		# E-2		#E-1		# B-3		# B-2		LOCATION TO			ISHIP	PROJECT NAME:
PIPE		Е		В		В		т	T	>		PIPE		>		Е		В		В		В	STRUCT		\dagger	Н	+
0 00		0.25		0.10		0.15	T	0.06	T	0.004		0.02		0.03		0.20		0.10		0.13		0.10	T AREA		t	NEP	R
0 00		0.60		0.81		0.87		0.84		0.11		0.99		0.69		0.72		0.90		0.72		0.81	RUNOFF "C" FACTOR			NEPTUNE	PRELIMNIARY
0000		0.150		0.081		0.131		0.050		0.0004		0.020	r	0.021	r	0.144		0.090		0.094		0.081	F CXA		t	11	ᅇᄃ
	0.861		0.711		0.131		0.500		0.0409	4	0.020		0.021		0.409	-	0.265		0.175	4	0.081		ACCUM		25		AL SITE
5	T	10		10		10	Ī	10		10		10	H	10	Ť	10		10	J.	10		10	All the second	IME	5 YR SI		P -
) h		25		25		25	H	25		25		25		25		25		25		25		25	TIME OF STORM CONC. FREQ. (MIN) (YRS)	QF C	ORM S	8	
8 90		6.80		6.80		6.80		6.80		6.80		6.80		6.80		6.80		6.80		6.80		6.80	RM INTEN	TIME OF CONCEN.	SEWER	COUNTY:	
2		1.02		0.55		0.89		0.34		0.0030		0.13		0.14		0.98		0.61		0.64		0.55	NCREM	W CF8	SYSTEM		SE ADVE
	5.86		4.84		0.89		3.40		0.28		0.13		0.14		2.78		1.80		1.19		0.55		"Q" TOTAL (CFS)		YR STORM SEWER SYSTEM COMPUTATIONS	MONMOUTH	FINAL SITE PLAN- GALILEE EGLISE ADVENTISTE PROPOSED CHURCH
	24		18		15		18		8		4		8		18		15		15		15		SIZE SIZE	+	SNOIT	HTU	OPOSE
	0.0050		0.0053		0.0050		0.0049		0.0100		0.0200		0.0100		0.0050		0.0050		0.0050		0.0050		SLOPE SLOPE				DCHURC
		0.013		0.013		0.013		0.013		0.010		0.010		0.010	- 52	0.013		0.013		0.013		0.013	MANN.	DESIGN			+
	16.04		7.66		4.58		7.37		1.58		0.35		1.58		7.45		4.58		4.58		4.58		"Q" FULL (CFS)		DATE: DEC	П	T
	10.18		2.83		3.69		3.97		1.30		0.22		1.43		4.67		2.78		3.39		4.03		"Q" VAR.	1	DEC 2	H	
	5.11		4.34		3.73		4.17		4.51		4.02		4.51		4.21		3.73		3.73		3.73		FULL Q (FPS)	1	2022	\top	1
	68		17		94		49		41		10		19		70		78		146		40		PIPE D LENGTH (FEET)			+	+
20 60		39.07		39.60		40.32		39.84		41.10		41.64		41.29		40.19		40.83		41.56		41.76	UPPER 'H INVERT ') (FEET)	PROFILE		CHECK	COMP
	38.73		39.51		39.85		39.60		40.69		41.44		41.10		39.84	ω.	40.44		40.83	O)	41.56	O)	LOWER INVERT	F	-	CHECKED BY:	TED BY
		45.00		44.70		44.70		45.55		46.10				46.10	*	44.80	4	45.10	ω	45.10	o	45.15	TOP ELEV (FEET)			BP	

	MH# 3		CO # 1	L	MH#2	L	R		# A-1		MH# 1		FROM	LOCATION				TOWNSHIP	TROJECT NAME:
FES#1		MH#3		MH#3		MH#2		MH#2		# A-1		MH # 1	70	ON				₽	NAME:
FES	M		8		M		PIPE		Þ		M		TYPE	STRUC					
	0.00		0.02		0.00		0.02		0.03		0.00		(Ac.)	AREA	T			NEPTUNE	באדר
	0.00		0.99		0.00		0.99		0.40		0.00		FACTOR	.C.	anonia			UNE	MNIAKY
	0.000		0.020		0.000		0.020	Γ	0.012		0.000		INCR		CYA				& FINA
0.933		0.020		0.913		0.020		0.893		0.881		0.020	ACCUM	ş	CVA		25		LSILEFI
	10		10		10		10		10		10		(NIN)	CONC.	MEGIE GUODA	TIME OF CONCEN.	YR STOP		AN- GA
	25		25		25		25		25		25		(YRS)	FREQ.	Medicass	FCON	SE W	COUNTY:	
	6.80		6.80		6.80		6.80		6.80		6.80		(IN/HR)	7	NE AN	CEN.	WER S	TY:	EGLISE
	0.00		0.13		0.00		0.13		0.08		0.00		(CFS)	INCREM.	**************************************	Q (CFS)	YSTEM C		- AUVEN
6.34		0.13		6.21		0.13		6.07		5.99		0.13	(CFS)	TOTAL	aQu.		25 YR STORM SEWER SYSTEM COMPUTATIONS	MONMOUTH	PRELIMNIARY & FINAL SITE PLAN- GALILEE EGLISE ADVENTISTE PROPOSED CHURCH
24		4		24		4		24		24		4	(INCH)	SIZE	adio	F	SNOI	UTH	POSEL
0.0053		0.0200		0.0050		0.0200		0.0051		0.0050		0.0200	(FT/FT)	SLOPE	zala				CHURCH
	0.013		0.010		0.013		0.010		0.013		0.013		"U"	MANN.		DESIGN			Ī
16.57		0.35		16.04		0.35		16.19		16.04		0.35	(CFS)	E.	aQu.	N	DATE: DEC		
10.22		0.22		9.83		0.22		10.11		10.05		0.22	(CFS)	VAR	aOa	1	DEC 2022		
5.27		4.02		5.11		4.02		5.15		5.11		4.02	(FPS)	FULLQ	WE		22		
15		19		38		æ		55		36		9	(FEET)	LENGTH	alala	-7			
	38.08		40.08		38.27		40.05	Г	38.55		38.73		(FEET)	INVERT	dadall	PROFILE		CHECKED BY:	COMPU
38.00		39.70		38.08		39.89		38.27		38.55		40.34	(FEET)	INVERT	damoi	т		ED BY:	I٦
	45.80	Γ	45.90		46.30	Γ		Γ	45.20	Γ	46.00	Γ	(FEET)		TOB			BP	_

B		# E-3		# B-5		# B-4		# E-2		# A-2		R		#A-3		#E-1		# B-3		# B-2		# B-1	LOCATION			TOWNSHIP	PROJE
	MH# 1		#E-3		# B-5		# B-5		#E-2		#A-2		# A-2		#E-2		#E-1		# B-3		#B-2		TO NOI			₹	PROJECT NAME:
PIPE		ш		В		В		ш		>		PIPE		Þ		ш		В		В		В	STRUCT		T		
0.02		0.25		0.10		0.15		0.06		0.004		0.02		0.03		0.20		0.10		0.13		0.10	AREA (Ac.)		T	NEPTUNE	RE
0.99		0.60		0.81		0.87		0.84		0.11		0.99		0.69		0.72		0.90		0.72		0.81	RUNOFF "C" FACTOR			UNE	IMNIAR
0.020		0.150		0.081		0.131		0.050		0.0004		0.020	Г	0.021		0.144		0.090		0.094		0.081	INCR CXA		T		/ & FINA
	0.861		0.711		0.131		0.500		0.0409		0.020		0.021		0.409		0.265		0.175		0.081		ACCUM		10		L SITE P
10		10		10		10		10		10		10		10		10		10		10		10	CONC.	IME	0 YR SI		LAN- G
25		25		25		25		25		25		25	Г	25		25		25		25		25	FREQ. (YRS)	TIME OF CONCEN.	ORMS	COUNTY:	ALILEE
8.00		8.00		8.00		8.00		8.00		8.00		8.00		8.00		8.00		8.00		8.00		8.00	(INJEN	NCEN.	EWER	NTY:	EGLIS
0.16		1.20		0.65		1.04		0.40		0.0035		0.16		0.17		1.15		0.72		0.75		0.65	"Q" INCREM. (CFS)	G (CFS)	100 YR STORM SEWER SYSTEM COMPUTATIONS		PRELIMNIARY & FINAL SITE PLAN- GALILEE EGLISE ADVENTISTE PROPOSED CHURCH
	6.89		5.69		1.04		4.00		0.33		0.16		0.17		3.27		2.12		1.40		0.65		TOTAL (CFS)		COMPUTA:	HTUOMNOM	ISTE PRO
	24		18		15		18		8		4		œ		8		15		15		15		(INCH)		SNOI	HTL	POSE
	0.0050		0.0053		0.0050		0.0049		0.0100		0.0200		0.0100		0.0050		0.0050		0.0050		0.0050		SLOPE SHOPE				CHURC
0.010		0.013		0.013		0.013		0.013		0.010		0.010		0.010		0.013		0.013		0.013		0.013	MANN.	DESIG			╗
	16.04		7.66		4.58		7.37		1.58		0.35		1.58		7.45		4.58		4.58		4.58		(CFS)	SIGN	DATE: DEC		П
	9.15		1.97		3.54		3.37	27 89	1.25		0.19		1.41		4.18		2.46		3.18		3.93		CFS)		DEC 2022		П
	5.11		4.34		3.73		4.17		4.51		4.02		4.51		4.21		3.73		3.73		3.73		FULL Q (FPS)	٦	22		\parallel
	68		17		94		49		41		10		19		70		78		146		40		PIPE LENGTH (FEET)	_			\parallel
40.52		39.07		39.60		40.32		39.84		41.10		41.64		41.29		40.19		40.83		41.56		41.76	UPPER INVERT (FEET)	PROFILE	7	CHECKED BY:	COMPU
	38.73		39.51		39.85		39.60		40.69		41.44		41.10		39.84		40.44		40.83	_	41.56		LOWER INVERT (FEET)	it		ED BY:	COMPUTED BY:
	- No. 100 -	45.00		44.70		44.70		45.55		46.10				46.10		44.80		45.10		45.10		45.15	TOP ELEV (FEET)			₽P	

	MH# 3		CO # 1		MH#2		RD	L	# A-1		MH# 1		FROM	LOCATION		
FES#1		MH#3		MH#3		MH# 2		MH#2		# A-1		MH # 1	TO	ON		
FES	<u>S</u>	T	8		<u>S</u>		PIPE	Γ	>	Γ	M	Γ	TYPE	STRUCT	T	
	0.00		0.02		0.00		0.02		0.03	T	0.00		-	AREA		
	0.00		0.99		0.00		0.99		0.40		0.00		FACTOR	RUNOFF		
	0.000		0.020		0.000		0.020	Γ	0.012		0.000	Γ	INCR	СХА		
0.933		0.020		0.913		0.020		0.893		0.881		0.020	ACCUM	CXA		10
	10		10		10		10	T	10		10	T	(MIN)	TIME OF	TIME	0 YR ST
	25	T	25		25		25		25	T	25	T	-	F STORM	TIME OF CONCEN.	ORM S
	8.00		8.00		8.00		8.00		8.00		8.00			A INTEN.	VCEN.	EWER :
	0.00		0.16		0.00		0.16		0.10		0.00		(CFS)	"Q"	Q (CFS)	SYSTEM
7.46		0.16		7.30		0.16		7.15		7.05		0.16	(CFS)	"Q"		100 YR STORM SEWER SYSTEM COMPUTATIONS
24		4		24		4		24		24		4	(INCH)	PIPE	T	SNOIL
0.0053		0.0200		0.0050		0.0200		0.0051		0.0050		0.0200	(FT/FT)	SLOPE	1	
	0.013		0.010		0.013		0.010		0.013		0.013		"a"	MANN	DESIGN	
16.57		0.35		16.04		0.35		16.19		16.04		0.35	(CFS)		SN	DATE: DEC
9.10		0.19		8.74		0.19		9.04		8.99		0.19	(CFS)	VAR.	1	DEC 2022
5.27		4.02		5.11		4.02		5.15		5.11		4.02	(FPS)	VET.	1	22
15		19		38		8		55		36		9		PIPE		
	38.08		40.08		38.27		40.05		38.55		38.73		5000 ACCORD	UPPER	PROFILE	
38.00		39.70		38.08		39.89		38.27		38.55		40.34		LOWER	im	
	45.80	T	45.90		46.30				45.20		46.00	Г		TOP		П

PROJECT- Galilee Eglise Adventiste Inc NUMBER- 1943A BY-BP DATE- 12/14/2022

CONDUIT OUTLET PROTECTION CALCULATIONS

TAILWATER < 0.5 x Do

24 " RCP -FES#1

 $D_0 = 2.00$

 $Q_{(25)} = 6.34 \text{ CFS}$

TW = 0.40 (0.2 Do ASSUMED)

 W_o = 2.00 (Width of culvert @ widest point)

3.17 CFS/ft (Q/Wo)

LENGTH OF APRON

1.8 x q

 $L_a = ---- +7 \times (D_0) =$

18.03 FEET

 $D_0^{1/2}$

USE

20.0 FEET

WIDTH OF APRON

 $W = (3 \times W_0) + La$

24.03 FEET

USE

25.0 FEET

RIPRAP SIZE

0.016

D₍₅₀₎ = ---- q ^ 4/3 = 2.24 INCHES

Tw

USE 3.0 INCHES

APRON THICKNESS

 $T = 2 \times D$ (50) w/FILTER FABRIC $T = 3 \times D$ (50)

0.50 FEET

0.75 FEET

USE

1 FT

USE

X



PROJECT- Galilee Eglise Adventiste Inc.

PROJECT NUMBER- 1943A

BY-BP

DATE- 12/14/2022

PREFORMED SCOUR HOLE CALCULATIONS

TAILWATER > 0.5 x Do

24 " RCP FES#1

 $D_0 =$ 2.00

Y=2.00

Q₍₁₀₀₎ = 7.46 CFS TW = 0.78 2 Yr water surf elev. - Inv of Inlet Pipe = 38.78 - 38.00 Width of culvert @ widest point)

3.73 CFS/ft (Q/Wo) q=

RIPRAP SIZE

$$D_{(50)} = ------ q^4/3 =$$

0.73 INCHES

Tw

USE 2.0 INCHES

APRON THICKNESS

$$T = 2 \times D$$
 (50) w/ FILTER FABRIC

0.33 FEET

USE

1.00

New Jersey Department of Agriculture

Hydrologic Modeling Database - Data Entry Form

Project Site Details
Chpt. 251 Application Number:
Start Date (if known): Summer 2023
County: Monmouth
Street Address: 3313 State Highway Route 33
Municipality: Neptune Township
Block: 3301
Lot: <u>4</u>
NJDEP Anderson Landuse Code (4 digits):
Landuse description:
Site Centroid Location (NJ State Plane Feet): 1
Northing: 501,471 Easting: 612,020
Project Contact Details Applicant: Galilee Eglise Adventiste Inc Address: 3313 State Highway Route 33
Phone: 732 822 8767 Email: lavarin1961@yahoo.com
Phone: 732 822 8767
Phone: 732 822 8767
Phone: 732 822 8767 Email: lavarin1961@yahoo.com
Phone: 732 822 8767 Email: lavarin1961@yahoo.com Post Construction Operation & Maintenance: ²
Phone: 732 822 8767 Email: lavarin1961@yahoo.com Post Construction Operation & Maintenance: Party Name: Galilee Eglise Adventiste Inc
Phone: 732 822 8767 Email: lavarin1961@yahoo.com Post Construction Operation & Maintenance: Party Name: Galilee Eglise Adventiste Inc Address: 3313 State Highway Route 33

New Jersey Department of Agriculture

Hydrologic Modeling Database - Data Entry Form

Drainage Area(s) to Basin [note-include any bypass areas]⁶

Drainage Area Name	Drainage Area (acres)	Post- Development CN#	Percent Impervious	Time of Concentration (min)
	1.58	74	59%	6

Basin Outlet Structure(s)⁷

ID: Emergrency Overflow only. Basin fully exfiltrates 100 year storm event

End of Pipe Location: 8 Northing:

Easting:

Discharge Type ⁹ (weir, orifice, etc)	Dimensions (diameter, length)	Elevation (USGS)	Discharge ¹⁰ Coefficient	Equation Used ¹¹
Orifice (Grate)	4 ft x 4 ft	44.50	0.6	$Q = CoAg[(2gd)^0.5]$

New Jersey Department of Agriculture Hydrologic Modeling Database – Data Entry Form

Basin Outlet Structure(s)

ID:

End of Pipe Location: Northing:

Easting:

Discharge Type (weir, orifice, etc)	Dimensions (diameter, length)	Elevation (USGS)	Discharge Coefficient	Equation Used

Basin Stage-Discharge Rating Table 12

Elevation (USGS Feet)	Storage (Acre-Ft)	Total Outlet Structure Discharge (cfs)
38.00	0.00	0.00
45.00	0.64	10.56*
100 yr water surface elevation	n = 43 86 with 0 00 of diach	and the second of the second o

NJDEP BMP Water Quality Structures¹³

Type (rain garden, green roof, seepage pit etc)	Size	Size Units (cu ft, sq ft etc)	Northing (SPF)	Easting (SPF)
Infiltration Basin	0.64	ac-ft	501,471	612,020