# Stormwater Management Report

# St. George Greek Orthodox Church Cemetery Expansion

2508 West Bangs Avenue Tax Map Block 1402, Lot 2 Township of Neptune Monmouth County, NJ

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Prepared by:



KENNEDY CONSULTING ENGINEERS, L.L.C.

211 MAPLE AVENUE RED BANK, NJ 07701 PHONE: 732.212.9393 • FAX: 732.212.9399

COA: 24GA28049700



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### Introduction

The applicant proposes the expansion of an existing cemetery located at 2508 West Bangs Road in Neptune Township. The expansion consists of the addition of grave plots, the extension of the onsite circulation roadway, as well as the construction of an enclosed refuse area and topsoil stockpile area. Ancillary improvements, including street trees, grading, and retaining walls are proposed. This stormwater management report is prepared to address the stormwater management requirements of the Township Land Development Ordinance and is prepared in accordance with standard engineering practices. This report contains the comparison and calculation of peak stormwater runoff flow rate at one point of comparison and includes the design of a porous pavement system to intercept and infiltrate runoff generated on-site. This report provides calculations showing no adverse impact from stormwater runoff as a result of this development as proposed.

### **Existing Site Conditions**

The parcel is approximately 5.25 acres in size and is on West Bangs Avenue in the Township of Neptune. The northern portion of the parcel is developed with a cemetery associated with St. George Greek Orthodox Church. The southern half is moderately wooded. Topographic information shown on the survey indicates the site slopes from a high point of about +122 feet in the north-central site area to approximately elevation +96 feet adjacent to Cheswick Court to the south, and elevation +115 feet at West Bangs Avenue to the north. Based upon this topography, all stormwater generated on-site is directed toward either the rear of the site (Cheswick Court) or toward the front (West Bangs Avenue). These points of comparison and associated drainage areas are shown on the enclosed Drainage Area Map. Soil survey mapping performed by the United States Department of Agriculture indicates that this parcel is underlain by Evesboro formation sands. This mapping unit is assigned to a hydrologic soil group (HSG) of A. HSG A soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission and are especially conducive to on-site stormwater infiltration practices.

## Proposed Development

The applicant proposes to expand the existing cemetery toward the south in order to both provide for additional burial plots and accessory storage areas for refuse and soil stockpiling. In order to facilitate the expansion, the existing looped roadway would be continued and expanded to the south. The proposed drainage patterns will remain as under existing conditions. That is, stormwater runoff generated on the southern portion of the site will continue to flow toward Cheswick Court (Drainage Area A). Stormwater runoff generated from the northerly western portion of the site will continue to flow toward West Bangs Avenue. Since no changes to the northern portion of the property are proposed, stormwater runoff to this point will remain unchanged. As such, the stormwater analysis calculations herein are performed at the rear of the property to provide an analysis of the change of runoff directed toward Cheswick Court.

In order to control the peak runoff flow rate of stormwater from the developed site, a permeable pavement system is proposed. Permeable paving is proposed for the expanded looped vehicular circulation roadway through the southern portion of the property. The porous pavement system will not only intercept runoff from precipitation that falls on the surface but is also designed to intercept runoff upstream of the pavement. The permeable pavement system consists of a bituminous asphalt open graded friction course, with a secondary porous pavement section below. Beneath the bituminous asphalt, a stone storage bed is proposed. The stone storage bed is sized to store runoff water for all design storms analyzed based upon the tested permeability rates of the in-situ soils, using a factor of safety of 2.0. Based upon the peak flow rate analysis of the design point and the maintenance of the existing flow paths, there will be an overall decrease in peak flow rates to the Point of Comparison at Cheswick Court. This result is expected as much of stormwater runoff from the developed surfaces is directed toward the permeable pavement system, and is allowed to infiltrate into the soils, instead of being conveyed to the south as surface runoff. The design of the permeable pavement system is contained within the appendix of this report.

## Stormwater Management Methodology

Pursuant to the Township of Neptune Land Development Ordinance, a "Major Development" is classified as one where one acre or more of land is disturbed. Since the project's limit of disturbance is greater than one acre, this project is classified as a "Major Development". As such, a permeable pavement system is designed to manage the increase in peak flow rates for the 2-, 10-, and 100-year storm events.

Specifically, the requirements for groundwater recharge (Section 528.3.F.1.b.(1).(b)) are met through the analysis of the minimum groundwater recharge volume comparison of pre vs. post construction runoff volume generated by the 2-year, 24-hour storm. To assess the peak rate of runoff requirements at Section 528.3.F.c.(1), this report takes a point-by-point comparative approach in determining the affect of stormwater runoff as a result of this development. After determining the stormwater runoff drainage areas, parameters and points of concern, the direct calculation of peak stormwater runoff from the drainage area under existing and proposed conditions is calculated.

#### Non-Structural and Structural Stormwater Management Strategies

In accordance with the Township ordinance, both structural and non-structural design techniques are designed into the project. These strategies include the following:

#### Non-Structural Stormwater Management Strategies (NJAC 7:8-5.3) utilized in this development:

- Protect areas that provide water quality benefits or areas susceptible to erosion
   To the greatest extent possible, the existing on-site wooded areas along the perimeter of the site are to remain undisturbed.
- Minimize impervious surfaces and/or disconnected the flow of runoff over impervious surfaces
   The stormwater runoff generated from the looped access areas are constructed of porous asphalt pavement.
   Therefore, no stormwater runoff will be generated within these areas, thus mitigating the impacts of added
   impervious surface.
- Maximize the protection of natural drainage features and vegetation
   To the greatest extent possible, the existing on-site wooded areas along the perimeter of the site are to remain
   undisturbed.
- 4. Minimize the decrease in the Time of Concentration from Pre- Construction to Post –Construction developments:

The developed Tc paths are over grassed areas and are lengthened and maximized to the greatest extent practicable.

#### 5. Minimize Land Disturbance including Clearing and Grading:

To the greatest extent possible, the existing on-site wooded areas and the perimeter of the site are to remain undisturbed.

6. Minimize Soil Compaction:

A note is added to the plan to address this concern.

7. **Provide Low Maintenance Vegetation:** Addressed on the landscaping plan.

#### 8. **Provide Pollutant Source Controls:**

A note outlining the requirements for fertilizer application, as outlined in the State's Standard for Permanent Vegetative Cover for Soil Stabilization, is included in the Soil Erosion Control Specifications.

#### Structural Stormwater Management Strategies (NJAC 7:8-5.7)

Structural strategies are incorporated into this project to meet the required Stormwater Quality Standards (NJAC 7:8- 5.5), Groundwater Recharge, and Stormwater Quantity Standards (NJAC 7:8- 5.4).

#### **Stormwater Quality Standards**

The porous pavement system is designed to provide the required reduction of the Total Suspended Solids (TSS). In accordance with section 9.7 of the New Jersey Stormwater Best Management Practices, the New Jersey Department of Environmental Protection indicates that permeable asphalt systems achieve 80% TSS removal. In order for a permeable asphalt pavement system to achieve an 80% TSS removal rate, certain construction requirement are required. These requirements are also shown on the proposed plans. In addition, a storage bed must be provided under the permeable asphalt paving system. The design of this storage bed is provided within the appendix of this report and is specified on the site plans for this project.

#### **Groundwater Recharge Requirements**

Calculations included herein show the analysis of the pre vs. post condition groundwater recharge for the 2 year, 24-hour storm event. The calculations indicate that the change in runoff volumes during the required design storm is 987 cubic feet of runoff. Under the

developed condisions, and in consideration of the proposed porous pavement system, approximately 1,511 cubic feet of runoff will be infiltrated. Since the predeveloped groundwater recharge is exceeded by approximately 165%, the groundwater recharge standard of the Township ordinance is met.

### **Runoff Peak Flow Rate**

Under predeveloped conditions, one drainage area is used to determine the rate of stormwater runoff flow from the site towards Cheswick Court (Point A). As described above and shown on the enclosed drainage area map, **Drainage Area A** consists of the on-site area tributary to **Point A**. To quantitatively assess the amount of existing stormwater runoff conveyed to **Point A**, the USDA TR-55 Unit Hydrograph Method is used. The hydrologic parameters are determined as required by standard engineering practice using the worksheets enclosed within the appendix of this report. These procedures are applicable in small watersheds, especially urbanizing watersheds, in the United States. First issued by the Soil Conservation Service (SCS) in January 1975, Technical Release 55 is consistent with the current engineering standard of practice.

Under developed conditions, one drainage area is used similar to the existing conditions of the site. This single developed drainage area is used to determine the peak flow rate of stormwater runoff toward Cheswick Court under the conditions of the expanded cemetery. As under existing conditions, **Drainage Area A** consists of the area tributary to **Point A**. This drainage area and design point is shown on the enclosed Drainage Area Map.

Storm events with return frequencies of 2, 10, and 100 years are included in the peak flow computations shown in the report appendix. The TR-55 methodology is utilized for determining the times of concentration (Tc) with a minimum time of concentration of 10 minutes.

As a result of the proposed re-development of the dry detention basin, the peak stormwater flow rate analysis shows a decrease from pre-developed rates of runoff for the comparison point at Cheswick Court for all design storm events analyzed. These results are illustrated in the tables shown in the conclusion and are consistent with the design of the proposed development. As such, the peak flow rate requirements of the ordinance are met.

## **Evaluation of Subsurface Soils**

Soil survey mapping performed by the United States Department of Agriculture indicates that this parcel is underlain by Evesboro formation sands. This mapping unit is assigned to a hydrologic soil group (HSG) of A. HSG A soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission and are especially conducive to on-site stormwater infiltration practices. In addition to this generally available soil mapping information, a site-specific soils investigation was undertaken. This soils investigation consisted of the excavation of five test pits to a depth of 10 to 10.5 feet below grade. In addition, fourteen replicate tube samples for laboratory analysis of soil permeability were collected and processed at a soil laboratory. The analysis yielded an average permeability rate of 9 inches per hour. Both the USDA soil survey report and site-specific soils study are included in the appendix of this report.

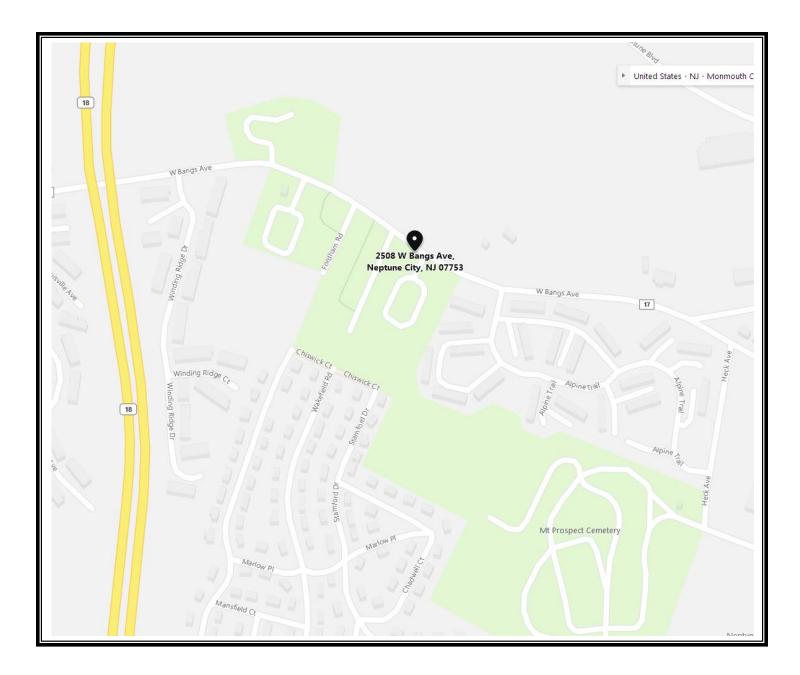
## Conclusion

The table below shows the comparison of peak stormwater runoff flow rates for the existing condition and proposed conditions towards Cheswick Court (**Point A**). This comparative analysis shows a reduction in the peak stormwater runoff flow rates from the developed site directed to the design point for the 2, 10, and 100-year design storm events. In addition, and as detailed above, groundwater recharge and stormwater quality is also achieved as required by the Township Land Development Ordiinance. As such, no adverse impacts due to stormwater runoff flow rates are expected as a result of the development of this site as proposed.

Design Storm	Existing (cfs)	Proposed (cfs)	Change in runoff
2 Year	0.04	0.03	-25%
10 Year	0.99	0.76	-23%
100 Year	8.7	7.6	-13%

## Appendices

## A | Location and Informational Mapping



**Location Map** 



## **B** | Soils Information



United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Monmouth County, New Jersey

St. George Cemetery



## Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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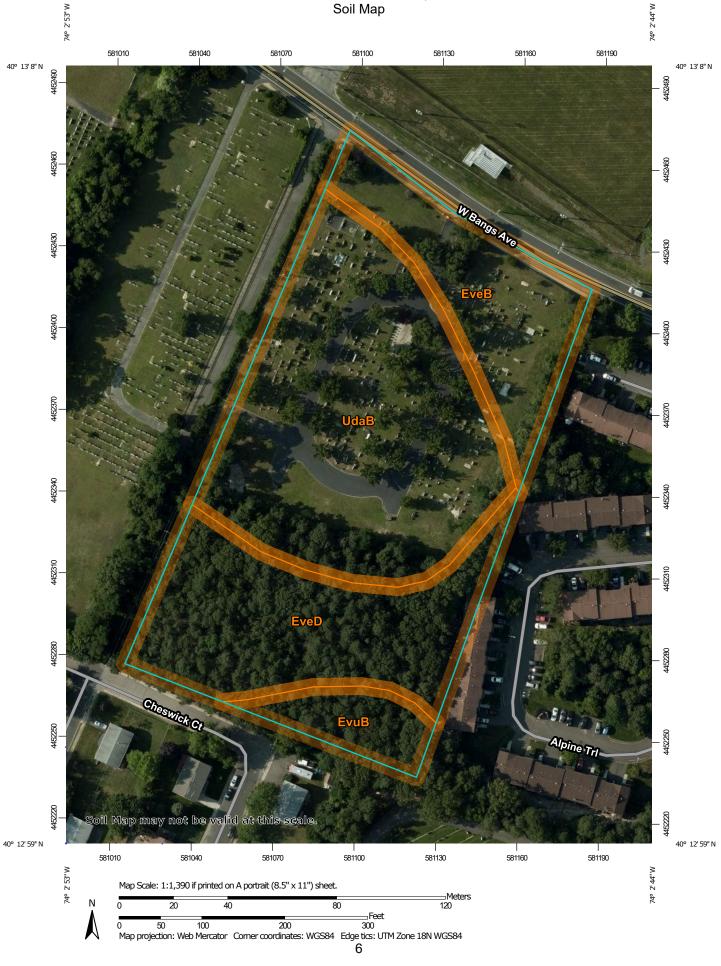
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## Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

#### Custom Soil Resource Report Soil Map



MAP INFORMATION The soil surveys that comprise your AOI were mapped at	Warning: Soil Map may not be valid at this scale.	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.	Please rely on the bar scale on each map sheet for map measurements.	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.	This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Monmouth County, New Jersey Survey Area Data: Version 13, Sep 16, 2019	Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jun 26, 2019—Jun 29, 2019	The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.
Area of Interest (AOI)	Area of Interest (AOI)  And Stony Spot Soils Soil Map Unit Polygons Wet Spot	eatu	Borrow Pit Streams and Canals Canads Canals Canads Canals Canads	<ul> <li>Closed Depression</li> <li>A Gravel Pit</li> <li>US Routes</li> <li>Gravelly Spot</li> <li>Major Roads</li> </ul>	<ul> <li>Landfill</li> <li>Lava Flow</li> <li>Background</li> <li>Marsh or swamp</li> <li>Aerial Photography</li> <li>Mine or Quarry</li> </ul>	<ul> <li>Miscellaneous Water</li> <li>Perennial Water</li> <li>Rock Outcrop</li> <li>Saline Spot</li> </ul>	<ul> <li>Sandy Spot</li> <li>Severely Eroded Spot</li> <li>Sinkhole</li> <li>Slide or Slip</li> </ul>	Sodic Spot

Map Unit Symbol Map Unit Name		Acres in AOI	Percent of AOI	
EveB	Evesboro sand, 0 to 5 percent slopes	1.0	18.5%	
EveD	Evesboro sand, 10 to 15 percent slopes	1.5	27.6%	
EvuB	Evesboro-Urban land complex, 0 to 5 percent slopes	0.3	6.1%	
UdaB	Udorthents, 0 to 8 percent slopes	2.6	47.8%	
Totals for Area of Interest	l	5.4	100.0%	

## Map Unit Legend

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

### Monmouth County, New Jersey

#### EveB—Evesboro sand, 0 to 5 percent slopes

#### **Map Unit Setting**

National map unit symbol: 4j74 Elevation: 0 to 150 feet Mean annual precipitation: 28 to 59 inches Mean annual air temperature: 46 to 79 degrees F Frost-free period: 161 to 231 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Evesboro and similar soils:* 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Evesboro**

#### Setting

Landform: Low hills Landform position (three-dimensional): Interfluve, side slope Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy eolian deposits and/or sandy fluviomarine deposits

#### **Typical profile**

A - 0 to 4 inches: sand AB - 4 to 17 inches: sand Bw - 17 to 31 inches: sand C - 31 to 80 inches: stratified loamy sand to sand

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (2.00 to 20.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 4.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: A Hydric soil rating: No

#### **Minor Components**

#### Atsion

Percent of map unit: 5 percent Landform: Flats Landform position (two-dimensional): Footslope Landform position (three-dimensional): Dip, talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### Lakehurst

Percent of map unit: 5 percent Landform: Flats, depressions Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear, concave Across-slope shape: Linear, concave Hydric soil rating: No

#### Mullica, rarely flooded

Percent of map unit: 5 percent Landform: Flood plains, drainageways, depressions Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear, concave Across-slope shape: Linear, concave Hydric soil rating: Yes

#### Downer

Percent of map unit: 5 percent Landform: Low hills, knolls Landform position (three-dimensional): Interfluve Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

#### EveD—Evesboro sand, 10 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 4j76 Elevation: 10 to 450 feet Mean annual precipitation: 28 to 59 inches Mean annual air temperature: 46 to 79 degrees F Frost-free period: 161 to 231 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Evesboro and similar soils:* 95 percent *Minor components:* 5 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Evesboro**

#### Setting

Landform: Dunes, low hills Landform position (three-dimensional): Interfluve, side slope *Down-slope shape:* Convex, *Across-slope shape:* Convex, linear *Parent material:* Sandy eolian deposits and/or sandy fluviomarine deposits

#### **Typical profile**

A - 0 to 5 inches: sand
Bw - 5 to 28 inches: loamy sand
C - 28 to 60 inches: stratified loamy sand to sand

#### **Properties and qualities**

Slope: 10 to 15 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (2.00 to 20.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 4.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: A Hydric soil rating: No

#### **Minor Components**

#### Downer

Percent of map unit: 5 percent Landform: Low hills, knolls Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### EvuB—Evesboro-Urban land complex, 0 to 5 percent slopes

#### Map Unit Setting

National map unit symbol: 4j78 Elevation: 10 to 150 feet Mean annual precipitation: 28 to 59 inches Mean annual air temperature: 46 to 79 degrees F Frost-free period: 161 to 231 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Evesboro and similar soils:* 60 percent *Urban land:* 30 percent *Minor components:* 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Evesboro**

#### Setting

Landform: Low hills Landform position (three-dimensional): Interfluve, side slope Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy eolian deposits and/or sandy fluviomarine deposits

#### **Typical profile**

A - 0 to 4 inches: sand
AB - 4 to 17 inches: sand
Bw - 17 to 31 inches: sand
C - 31 to 80 inches: stratified loamy sand to sand

#### Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (2.00 to 20.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 4.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: A Hydric soil rating: No

#### Description of Urban Land

#### Setting

*Parent material:* Surface covered by pavement, concrete, buildings, and other structures underlain by disturbed and natural soil material

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

#### **Minor Components**

#### Lakehurst

Percent of map unit: 5 percent Landform: Flats, depressions Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear, concave Across-slope shape: Linear, concave Hydric soil rating: No

#### Downer

Percent of map unit: 5 percent Landform: Low hills, knolls Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### UdaB—Udorthents, 0 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 1j1jk Elevation: 400 to 1,500 feet Mean annual precipitation: 30 to 64 inches Mean annual air temperature: 46 to 79 degrees F Frost-free period: 131 to 178 days Farmland classification: Not prime farmland

#### Map Unit Composition

Udorthents and similar soils: 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Landform: Low hills Down-slope shape: Linear Across-slope shape: Linear Parent material: Fill and/or disturbed original soil material

#### **Typical profile**

A - 0 to 12 inches: loam C - 12 to 72 inches: loamy sand

#### **Properties and qualities**

Slope: 0 to 8 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Moderate (about 6.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: D Hydric soil rating: No

## Soil Information for All Uses

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

## Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

### Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

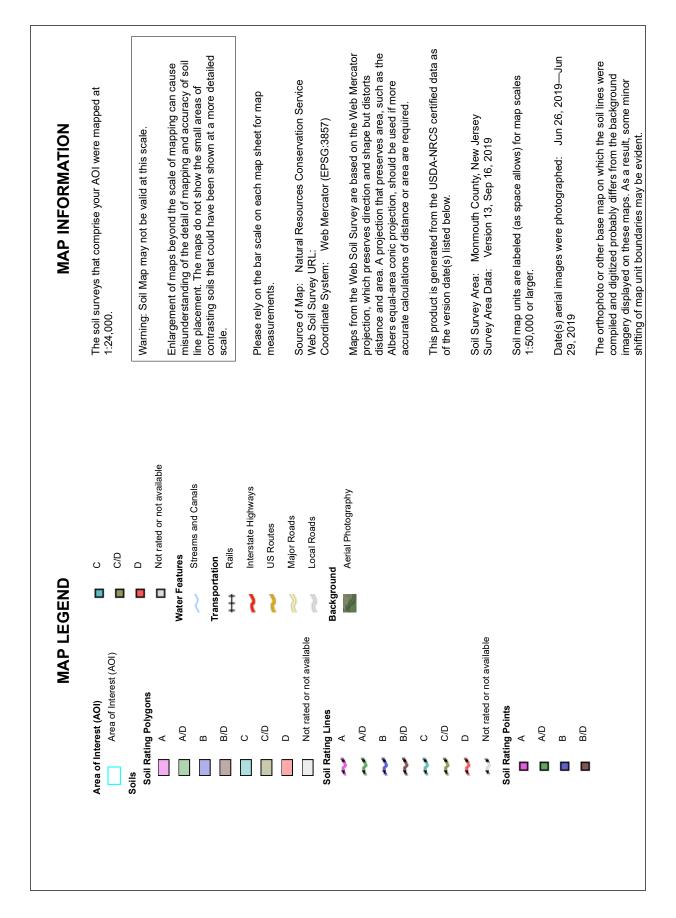
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

#### Custom Soil Resource Report Map—Hydrologic Soil Group





### Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
EveB	Evesboro sand, 0 to 5 percent slopes	A	1.0	18.5%
EveD	Evesboro sand, 10 to 15 percent slopes	A	1.5	27.6%
EvuB	Evesboro-Urban land complex, 0 to 5 percent slopes	A	0.3	6.1%
UdaB	Udorthents, 0 to 8 percent slopes	D	2.6	47.8%
Totals for Area of Inter	est	1	5.4	100.0%

### Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



Melick-Tully & Associates

A Division of GZA



SOIL LOGS/PERMEABILITY TESTS PROPOSED CEMETERY STORMWATER FACILITIES ST. GEORGE CREEK ORTHODOX CHURCH 2508 West Bangs Avenue Neptune, Monmouth County, New Jersey

January 21, 2020 File No. 26.0091995.00

**PREPARED FOR:** Kennedy Consulting Engineers, LLC 211 Maple Avenue Red Bank, NJ 07701

### Melick-Tully & Associates, A Division of GZA

117 Canal Road | South Bound Brook, NJ 08880 732-356-3400

GZA has 32 Offices Nationwide
www.melick-tully.com
www.gza.com

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Melick-Tully & Associates

A Division of GZA

GEOTECHNICAL ENVIRONMENTAL ECOLOGICAL WATER CONSTRUCTION MANAGEMENT

117 Canal Road South Bound Brook, NJ 08880 T: 732.356.3400 www.melick-tully.com www.gza.com January 21, 2020 File No. 26.0091995.00

Kennedy Consulting Engineers, LLC 211 Maple Avenue Red Bank, New Jersey 07701

Attention: Mr. James A. Kennedy, P.E. Vice President

Report Soil Logs/Permeability Tests Proposed Cemetery Stormwater Facilities Neptune, Monmouth County, New Jersey St. George Greek Orthodox Church

#### Introduction

This report presents the results of soil logs and permeability testing performed along a proposed loop driveway to be built to service an expansion of the existing St. George Cemetery in Neptune, Monmouth County, New Jersey. The cemetery is located at 2508 West Bangs Avenue. The site is situated between West Bangs Avenue and Cheswick Court. The site is designated as Lot 2, Block 1402 on Neptune Tax Map 41.02. The approximate location of the cemetery is shown on the Site Location Map, Plate 1. This report was prepared in general accordance with our proposal dated October 11, 2019.

#### **Proposed Construction**

The existing cemetery occupies the northern half of the site and is proposed to be expanded into the wooded southern half of the site. The new expansion will include construction of an extension of loop driveway through the center of the site. Testing



Eugene M. Gallagher, Jr., P.E., Principal Robert E. Schwankert, P.E., Principal Mark R. Denno, P.E., Principal Christopher P. Tansey P.E., Associate Principal Todd E. Horowitz, P.E., Associate Principal



January 21, 2020 File No. 26.0091995.00 St. George Greek Orthodox Church - Neptune Page 2

for stormwater facilities to accommodate porous pavement or below-grade infiltration facilities was to include test explorations advanced along the new driveway alignment at the beginning of the loop driveway at the edges of the woods and at intervals along the loop road.

#### **Purpose and Scope of Work**

The purpose of our services was to:

- 1) explore the subsurface soil and groundwater conditions at five locations within the expanded loop driveway alignment for the proposed expanded cemetery area;
- 2) collect soil samples of the subsoil layers for permeability testing;
- 3) summarize the nature of the soils encountered in the explorations and the permeability test results as they relate to the NJDEP Stormwater Design Requirements; and
- 4) provide a summary report of the findings for use by KCE in their evaluation and design of the stormwater facilities.

To accomplish these purposes, five test pits were performed at locations along the proposed loop driveway. The test pits were excavated using a John Deere 310SG rubber-tire backhoe and extended to depths of 10 to 10.5 feet below grade. Two test pits (Test Pits 1 and 5) were advanced along the new driveway alignment at the edge of the woods and three tests pits (Test Pits 2 through 4) were advanced within the woods along the loop driveway. The approximate locations of the test pits are shown on the Plot Plan, Plate 2.

All field work was performed under the direct technical observation of a geologist from MTA. Our representative located the explorations in the field, maintained continuous logs of the explorations as the work proceeded and collected selected bulk samples of the encountered materials. In addition,



relatively undisturbed tube samples were obtained from the test pits. Detailed Logs of Test Pits are presented on Plates 3A through 3E. The materials were visually described in general accordance with the USDA Soil Textural Chart described on Plate 4.

Samples of the native subsoils were collected from the test pits for laboratory gradation testing, the results of which are presented on Plate 5. Fourteen replicate tube samples of the subsoils were also subjected to laboratory tube permeameter permeability testing, the results of which are summarized on Plate 6. The results of the field and laboratory testing have provided the basis for our findings.

The following discussion of our findings are subject to the Limitations attached as an Appendix to this report.

#### **Site Conditions**

<u>Surface Features</u>: The subject property is an existing cemetery which occupies the northern half of the site. The southern half, where the test pits were advanced, is moderately wooded. Topographic information shown on the plan provided to us indicates the site grades slope from a high point of about Elevation +122 feet in the north-central site area to about Elevation +96 feet adjacent to Cheswick Court to the south, and Elevation +115 feet at West Bangs Avenue to the north. The surface grades in the vicinity of the test pits vary from about Elevation +120 to +112 feet.

<u>Subsurface Conditions</u>: Test Pits 1 and 5 encountered 3 and 2 inches of topsoil, respectively. Test Pits 2 through 4 encountered 1 to 2 inches of leaf litter at the surface. The topsoil in Test Pits 1 and 5 was



underlain by about 2 feet of sandy loam fill which was underlain by 2 to 6 inches of the original topsoil layer.

The surface and fill materials were underlain by stratified sand, loamy sand, and sandy clay loam soils which extended to the bottom of the test pits at depths of 10 to 10.5 feet. A 1.5-foot layer of silty clay was encountered in Test Pit 3 at a depth of 4.5 feet.

Groundwater was not observed to at least 10 feet in the test pits performed at the time of our study, (and deeper than Elevation +103 feet at Test Pit 3, the lowest elevated test pit) which were performed during the traditional high groundwater season, January through April. Few fine faint mottles which may possibly be an indicator of post-temporary or seasonal saturation, were noted at depths of about 3 to 5 feet in the test pits, with the exception of Test Pit 2 where mottling was not present to 10 feet. However, considering the site is elevated above the surrounding properties, the absence of prominent mottling, and that groundwater was not present in the sandy subsoils to more than 10 feet during the wet season, the faint mottles appear most likely to be relic, or possibly representative of natural color variegations rather than areal groundwater.

### **Permeability Test Results**

Tube permeameter permeability tests were performed on tube samples of the sandy and silty subsoils collected at depth from Test Pits 1 through 5. The permeability tests indicate the majority of the tested sand and loamy sand soils exhibited average permeabilities on the order of 1 to greater than 20 inches per hour and was more than 10 inches per hour in most cases. In Test Pits 3 through 5, the upper loamy



January 21, 2020 File No. 26.0091995.00 St. George Greek Orthodox Church - Neptune Page 5

sand, sandy clay loam, and silty clay soil layers that extended to 6 to 8 feet below grade exhibited lower

permeabilities. The results of the permeability tests are summarized on Plate 6.

Please contact us if you have any questions regarding this information.

The following Plates and Appendix are attached and complete this report:

Plate 1 – Site Location Map Plate 2 – Plot Plan Plates 3A through 3E – Logs of Test Pits Plate 4 – USDA Soil Textural Chart Plate 5 – Gradation Curves Plate 6 – Summary of Laboratory Permeability Test Results Appendix – Limitations

Respectfully submitted,

MELICK-TULLY and ASSOCIATES, a Division of GZA GeoEnvironmental, Inc.

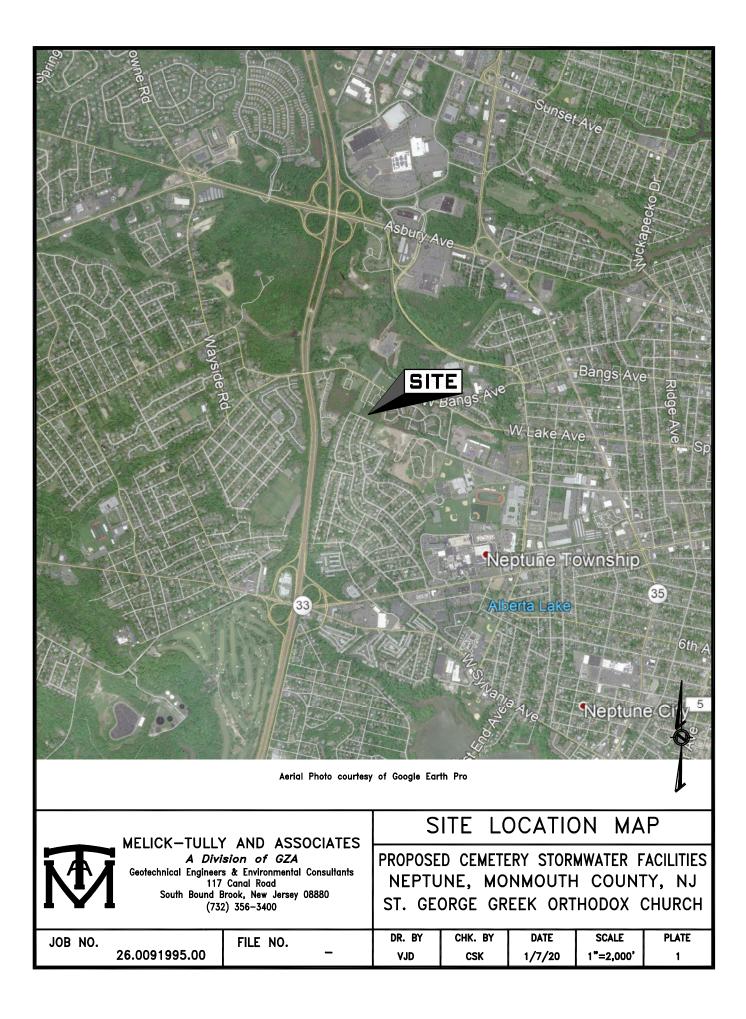
Cory S. Karinja, P.E. Associate Project Manager

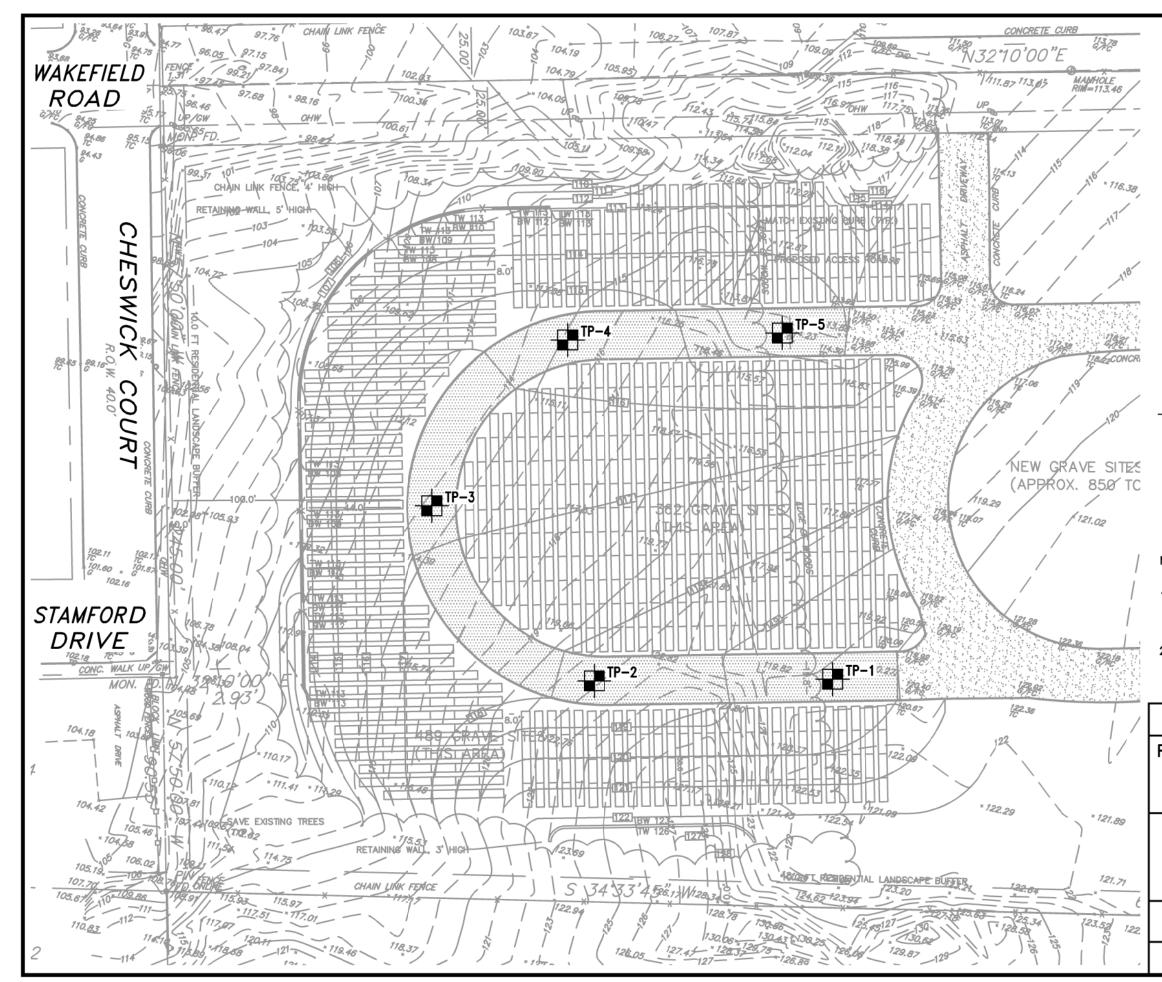
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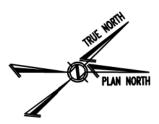
Mark R. Denno, P.E. Consultant/Reviewer

CSK:RES/csk (1 copy submitted via e-mail)

Robert E. Schwankert, P.E. Principal







KEY:



### NUMBER AND APPROXIMATE LOCATION OF TEST PITS PERFORMED FOR THIS STUDY

NOTES:

- This drawing is part of Melick—Tully and Associates, a Division of GZA, Report No. 26.0091995.00 and should be read together with the report for complete evaluation.
- General layout was obtained from a drawing prepared by 2. Kennedy Consulting Engineers, entitled "Site Layout Plan" dated 7/29/19, scale 1"=30'.

# PLOT PLAN

PROPOSED CEMETERY STORMWATER FACILITIES NEPTUNE, MONMOUTH COUNTY, NJ ST. GEORGE GREEK ORTHODOX CHURCH

₩ M	7	MELICK-TULLY AND ASSOCIATES <i>A Division of GZA</i> Geotechnical Engineers & Environmental Consultants 117 Canal Road South Bound Brook, New Jersey 08880 (732) 356-3400					
JOB NO.	26.0091995	5.00	FIL	E NO.	-		
DR. BY VJD	CHK. BY CSK		TE 7/20	SCALE 1"=40'	PLATE 2		

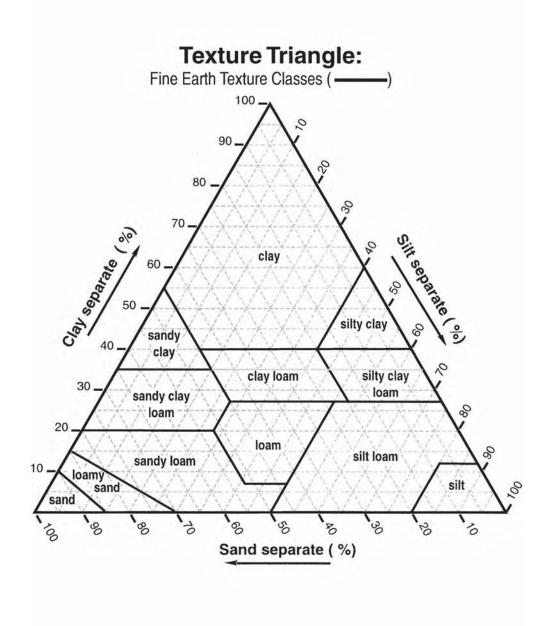
					TEST P	PIT LOG				
GZN		<b>ivision of</b> onmental, ad Scientists			-	k Orthodox Churc une, NJ	SHEET: PROJEC	RATION NO.: TP-1 1 of 1 CT NO: 26.0091995.00 VED BY: Cory Karinja		
Logged	<b>By:</b> Glenn Zr	nigrodski		Te	st Pit Location: Se	ee Plan	Final Test P	it Depth (ft.): 10		
Contractor: Operator:				Gro	ound Surface Elev	Finish: 1/2/2020 - 1/2/2	2020			
Type of I	Excavator:							ater Depth (ft.)	_	
Excavato	or Model:					Date 1/2/20	Time	Water Depth NE	Stab.Ti	me
Depth (ft)	Sample No.	Sample Depth (ft.)	Stratum Depth (ft.)	Symbol		Sample Descri	ption and Identific	ation	Water Content (%)	Remark
-			0-0.3					amy sand, weak fine		
1			0.3-1.8		-		-	ry, few fine roots reak fine granular,		
=	S1	1.5				brupt wavy bour				
2 _	51	1.5	1.8-2			oil - Dark brown	(10YR, 3/3) loa	my sand, weak fine	_	
-			2-5			st, loose, abrupt				
3 _						v (10YR, 7/6) loa st, loose, gradua				
	S2, T1	3.5			5,	, ,,,	5	5		
4 _										
5										
° –			5-8					ravel, single grain,		
6 _						clear wavy bound intered @ 60 inc		int gray (10YR, 6/1)		
-	S3, T2	6				0				
7										
-										
8 _			8-10		96"-120" Yello	w (10YR 8/8) k	amy sand 5%	gravel, single grain,	_	
					moist, loose, f	ew fine faint gray		ottles encountered		
9	S4, T3	9			@ 96 inches t	o 120 inches				
10										
					End of explora	ation at 10 feet.				
11 _					Groundwater	seepage not end	countered			
-					Mottling enco	untered @ 60"				
12					Note: Asphar	t layer encounter	red @ 2', test p	it moved 5' south		
-										
13 _										
14 _										
15										
RKS										
REMARKS										
R										
See Loa	Key for explo	ration of san	nple descripti	on and i	dentification proce	dures. Stratification	n lines represent	approximate Diat	e No.:3A	
boundarie times and	s between so under the co	il and bedroc nditions state	k types. Actu d. Fluctuatio	ial transit	ions mav be gradu	al. Water level reauter due to other fac	dings have been	made at the	5 110JA	
times the	measurement	s were made		-	-					

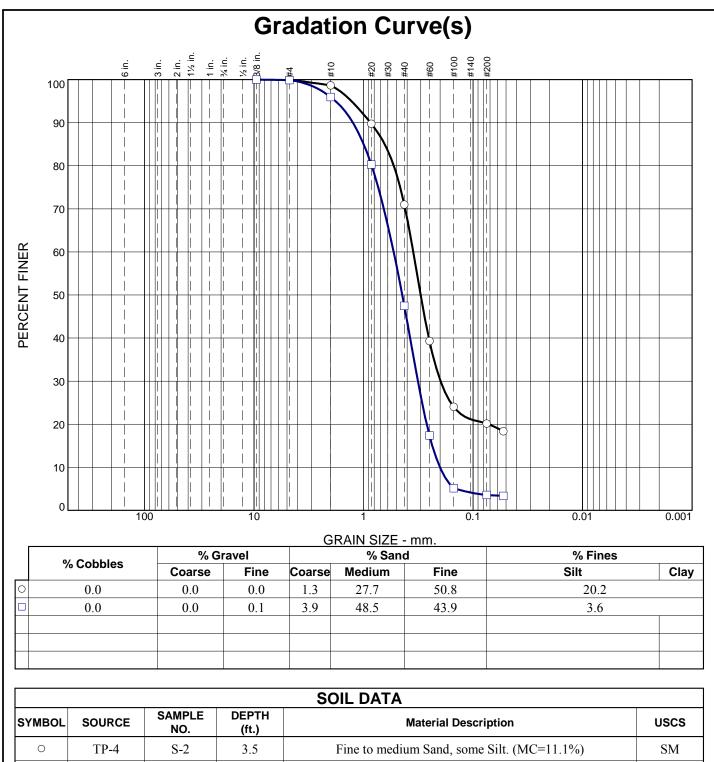
	TEST PIT LOG										
GZN	MTA, a D GeoEnvir Engineers an	onmental.	GZA Inc		-	k Orthodox Churc une, NJ	SH PF	(PLORATION NO.: HEET: 1 of 1 ROJECT NO: 26.009 EVIEWED BY: Cory	91995.00		
Logged	<b>By:</b> Glenn Zn	nigrodski/Sea	n Stevenson	Tes	st Pit Location: Se	Pit Location: See Plan Final Test Pit Depth (ft.): 10			10		
Contract Operator				Gro	ound Surface Elev	<b>v. (ft.):</b> 122.0	Date St	tart - Finish: 1/2/20	20 - 1/2/20	20	
Type of	Excavator:							undwater Depth (ft.)		_	
Excavate	or Model:					Date 1/2/20	Time	Water De	epth	Stab.Ti	me
Depth (ft)	Sample No.	Sample Depth (ft.)	Stratum Depth (ft.)	Symbol		Sample Descri	 ption and Ide	entification		Water Content (%)	Remark
			0-0.2		0"-2" Leaf litte			-l 00/		J	
	S1	1.5	0.2-2			abrupt smooth bo		d, 3% gravel, singl ew fine roots	e grain,		
2			2-10		24"-120" Brov single grain, n		YR, 6/6) loa	amy sand, 10% gı	ravel,	-	
4	S2, T1	3.5									
5_											
6	S3, T2	6									
8											
9 -	S4, T3	9									
10 _					End of explora	ation at 10 feet.					
11					Groundwater Mottling not e	seepage not enc ncountered	countered				
12 <u>-</u> - - - - - - - - - - - - - - - - - -											
13											
:0202/22/ 15											
3 - WI HEST PIT STRATUM LINES: 112 2002; 10:38:32 AM 14											
See Log boundarie times and times the	s between so	il and bedroc nditions state	k types. Actua d. Fluctuations	l transiti	ons mav be gradu	dures. Stratification Ial. Water level rea ur due to other fact	idinas have	been made at the	Plate	No.:3B	

	TEST PIT LOG											
GZN	MTA, a D GeoEnvir Engineers ar	<b>Division of</b> onmental, ad Scientists	GZA , Inc		-	k Orthodox Churc une, NJ	h	SHEET: PROJEC	ATION NO.: 1 of 1 T NO: 26.00 ED BY: Cory	91995.00		
Logged	By: Glenn Zr	nigrodski/Sea	an Stevenson	Tes	st Pit Location: S	ee Plan	Fin	al Test Pit	t Depth (ft.):	10		
Contrac Operato				Gro	Ground Surface Elev. (ft.): 114.0 Date Start - Finish: 1/2/2020 - 1/2/2020						20	
Type of	Excavator:								ter Depth (ft.	-		
Excavat	tor Model:					Date 1/2/20	1	ime	Water D	lepth	Stab.Ti	me
Depth (ft)	Sample No.	Sample Depth (ft.)	Stratum Depth (ft.)	Symbol		Sample Descri	ption an	d Identifica	ation		Water Content (%)	Remark
-	-		0-0.1		0"-1" Leaf litte		1			• .	J	
1	-		0.1-2			ray (10YR, 7/1) l wavy boundary,			gle grain, mo	oist,		
2_	S1	1.5	2-3		24"-36" Brow	nish yellow (10Yf	R 6/6)	loamv sa	nd 2% gray	vel	-	
3_	S2	2.5			single grain, n	noist, loose, clear	r wavy	boundary	/			
4	S3, T1	3.5	3-6		moderate me	nish yellow (10Ył dium subangular / fine faint gray (′ ′2 inches	block	y, moist, fi	irm, gradual	wavy		
5  6			6-10		72"-120" Ligh	t gray (10YR, 7/2	1) loam	iv sand 5	i% gravel si	ingle	-	
7	S4, T2	6.5			grain, moist, k		,	<b>,</b> , ,	5,	5		
9 - - 10	S5, T3	9										
-					End of explore	ation at 10 feet.						
11   12						seepage not end untered @ 36"	counte	red				
	-											
	-											
14 _	-											
15	-											
REMARKS												
boundari times an	Log Key for exploration of sample description and identification procedures. Stratification lines represent approximate daries between soil and bedrock types. Actual transitions may be gradual. Water level readings have been made at the s and under the conditions stated. Fluctuations of groundwater may occur due to other factors than those present at the s the measurements were made.											

	TEST PIT LOG											
GZN	MTA, a D GeoEnvir Engineers ar	onmental,			St. George Greek Orthodox Church Neptune, NJ			Sheet: Project	ATION NO.: 1 of 1 NO: 26.00 D BY: Cor	1 )91995.00		
Logged	I By: Glenn Zr	nigrodski		Tes	Test Pit Location: See Plan         Final Test Pit Depth (ft.): 10.5							
Contrac Operato				Gro	Ground Surface Elev. (ft.): 115.0 Date Start - Finish: 1/2/2020 - 1/2/2020							
Type of	Excavator:								er Depth (f	-		
Excava	Excavator Model:					Date 1/2/20	Tim	e	Water I NE		Stab.Ti	me
Depth (ft)	Sample No.	Sample Depth (ft.)	Stratum Depth (ft.)	Symbol		Sample Descri	tion and l	Identificat	ion		Water Content (%)	Remark
-	-		0-0.1			er, dark brown (10		,				
1_			0.1-1			ray (10YR, 3/1) k wavy boundary, f			e grain, m	oist,		
2	S1	1	1-4.5		12"-54" Brow	nish yellow (10YF pangular blocky, r	R, 6/6) sa	andy cla				
3_	- - -											
4 _	S2, T1	3.5										
5_	S3, T2	5	4.5-6		moderate me	nish yellow (10YF dium subangular v fine faint gray (1 72 inches	blocky, i	moist, fir	m, clear w	/avy		-
6 7			6-10.5			nt gray (10YR, 7/1	) loamy	sand, 29	% gravel, s	single	-	
8_	S4, T3	8										
9_	-											
	-											
11	-					ation at 10.5 feet						
12 _						seepage not end untered @ 54 ind		a				
13												
14	-											
15	]											
REMARKS												
boundari times an	es between so	il and bedroc nditions state	k types. Actu d. Fluctuatior	al transiti	ons mav be gradu	dures. Stratification ual. Water level rea our due to other fact	dinas hav	re been m	ade at the	Plate	No.:3D	

MTA, a Division of GZA GeoEnvironmental, Inc Engineers and Scientists					St. George Gree	PIT LOG k Orthodox Churcl une, NJ	SHEE PROJE	DRATION NO.: TP-5 T: 1 of 1 ECT NO: 26.0091995.00 WED BY: Cory Karinja		
Contract		nigrodski			Test Pit Location: See Plan         Final Test Pit Depth (ft.): 10.5           Ground Surface Elev. (ft.): 114.23         Date Start - Finish: 1/2/2020 - 1/2/20.					
Operator							Groundy	vater Depth (ft.)		
Type of E	Excavator:					Date	Time	Water Depth	Stab.Ti	me
Excavato	or Model:					1/2/20		NE		
Depth (ft)	Sample No.	Sample Depth (ft.)	Stratum Depth (ft.)	Symbol		Sample Descrip	otion and Identif	ication	Water Content (%)	
-			0-0.2					bamy sand, weak fine		Γ
1 1	S1	1.5	0.2-2		2"-24" FILL -	Brown (10YR, 4/3	3) sandy loam	ndary, few fine roots n, 5% gravel, weak fine dary, few fine roots		
2 _		1.0	2-2.5			oil - Dark brown ( st, loose, clear wa		amy sand, weak fine	_	
3 -	S2, T1	3.5	2.5-4.2		30"-50" Yellov		my sand, 7%	gravel, single grain,		
4 - 5	02,11	0.0	4.2-8		weak fine sub	angular blocky, n	noist, loose, c	clay loam, 5% gravel, lear wavy boundary, intered @ 50 inches		
6 _ 7 _	S3, T2	6			to 96 inches	gray (10113, 0/1)				
8 _ 9 _ -	S4, T3	9	8-10.5		grain, moist, le	t gray (10YR, 7/1 oose, few fine fair @ 96 inches to 1	nt gray (10YR	, 7% gravel, single , 6/1) mottles	_	
					End of explor	ation at 10.5 feet.				
11 _  12					Groundwater	seepage not enc untered @ 50"				
13 _										
14 _ - -										
15										
REMARKS										
See Log I boundarie	Key for explo	ration of san il and bedroo	nple description	on and id al transit	dentification proce tions may be gradu	dures. Stratification Jal. Water level read Jur due to other fact	lines represen dings have bee	t approximate n made at the present at the	e No.:3E	





			, , , , ,	
TP-4	S-4	8	Fine to medium Sand, trace Silt. (MC=4.3%)	SP

Melick-Tully & Associates	Client: Kennedy Consulting Engineers		
a Division of GZA GeoEnvironmental, Inc.	<b>Project:</b> Proposed Stormwater Facilities, Neptune City	', NJ	
South Bound Brook, NJ	Project No.: 26.0091995.00	Plate	5

## Summary of Laboratory Permeability Test Results Proposed Cemetery Stormwater Facilities Neptune, New Jersey St. George Greek Orthodox Church

Test Pit No.	Depth (feet)	Permea (inche	USDA Soil Classification	
INO.	(leet)	А	В	Classification
1	3.5	>20	>20	Loamy Sand
1	6.0	>20	>20	Loamy Sand
1	9.0	10.1	15.5	Loamy Sand
2	3.0	>20	>20	Loamy Sand
2	6.0	>20	>20	Loamy Sand
3	3.5	0.59	0.52	Sandy Clay Loam
3	6.5	1.5	0.23	Loamy Sand
3	9.0	12.7	16.5	Loamy Sand
4	3.5	2.3	2.9	Sandy Clay Loam
4	5.0	<0.06	<0.06	Silty Clay
4	8.0	18.7	>20	Loamy Sand
5	3.5	2.3	1.8	Loamy Sand
5	6.0	<0.06	<0.06	Sandy Clay Loam
5	9.0	12.3	>20	Loamy Sand

MELICK-TULLY AND ASSOCIATES, a Division of GZA GeoEnvironmental, Inc.

APPENDIX

#### APPENDIX

#### Limitations

#### A. Subsurface Information

<u>Locations</u>: The locations of the explorations were approximately determined by tape measurement from existing site features. Elevations of the explorations were approximately determined by interpolation between contours shown on topographic plans provided to us. The locations and elevations of the explorations should be considered accurate only to the degree implied by the method used.

<u>Interface of Strata</u>: The stratification lines shown on the individual logs of the subsurface explorations represent the approximate boundaries between soil types, and the transitions may be gradual.

<u>Field Logs/Final Logs:</u> A field log was prepared for each exploration by a member of our staff. The field log contains factual information and interpretation of the soil conditions between samples. Our recommendations are based on the final logs as shown in this report and the information contained therein, and not on the field logs. The final logs represent our interpretation of the contents of the field logs, and the results of the laboratory observations and/or tests of the field samples.

<u>Water Levels</u>: Water level readings have been made in the explorations at times and under conditions stated on the individual logs. These data have been reviewed and interpretations made in the text of this report. However, it must be noted that fluctuations in the level of the groundwater will occur due to variations in rainfall, temperature, and other factors.

<u>Pollution/Contamination</u>: Unless specifically indicated to the contrary in this report, the scope of our services was limited only to investigation and evaluation of the geotechnical engineering aspects of the site conditions, and did not include any consideration of potential site pollution or contamination resulting from the presence of chemicals, metals, radioactive elements, etc. This report offers no facts or opinions related to potential pollution/contamination of the site.

<u>Environmental Considerations</u>: Unless specifically indicated to the contrary in this report, this report does not address environmental considerations which may affect the site development, e.g., wetlands determinations, flora and fauna, wildlife, etc. The conclusions and recommendations of this report are not intended to supersede any environmental conditions which should be reflected in the site planning.

#### **B.** Applicability of Report

This report has been prepared in accordance with generally accepted soils and foundation engineering practices for the exclusive use of St. George Greek Orthodox Church for specific application to the design of the proposed cemetery stormwater facilities. No other warranty, expressed or implied, is made.

This report may be referred to in the project specifications for general information purposes only, but should not be used as the technical specifications for the work, as it was prepared for design purposes exclusively.

#### C. Reinterpretation of Recommendations

<u>Change in Location or Nature of Facilities:</u> In the event that any changes in the nature, design or location of the <u>facilities</u> are planned, the conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and conclusions of this report modified or verified in writing.

<u>Changed Conditions During Construction</u>: The analyses and recommendations submitted in this report are based in part upon the data obtained from 5 widely-spaced test pit excavations performed for this study. The nature and extent of variations between the explorations may not become evident until construction. If variations then appear evident, it will be necessary to reevaluate the recommendations of this report.

<u>Changes in State-of-the-Art:</u> The conclusions and recommendations contained in this report are based upon the applicable standards of our profession at the time this report was prepared.

#### D. Use of Report by Prospective Bidders

This soil and foundation engineering report was prepared for the project by Melick-Tully and Associates, a Division of GZA GeoEnvironmental Inc. (MTA) for design purposes and may not be sufficient to prepare an accurate bid. Contractors utilizing the information in the report should do so with the express understanding that its scope was developed to address design considerations. Prospective bidders should obtain the owner's permission to perform whatever additional explorations or data gathering they deem necessary to prepare their bid accurately.

#### E. Construction Observation

We recommend that MTA be retained to provide on-site soils engineering services during the earthwork construction and foundation phases of the work. This is to observe compliance with the design concepts and to allow changes in the event that subsurface conditions differ from those anticipated prior to the start of construction.

# C| Groundwater Recharge Calculations

ST. GEORGE CEMETERY, LOT 2, BLOCK 1402, NEPTUNE TOWNSHIP, MONMOUTH CO., NJ

## SPREADSHEET ANALYSIS OF STORM WATER DRAINAGE CALCULATIONS

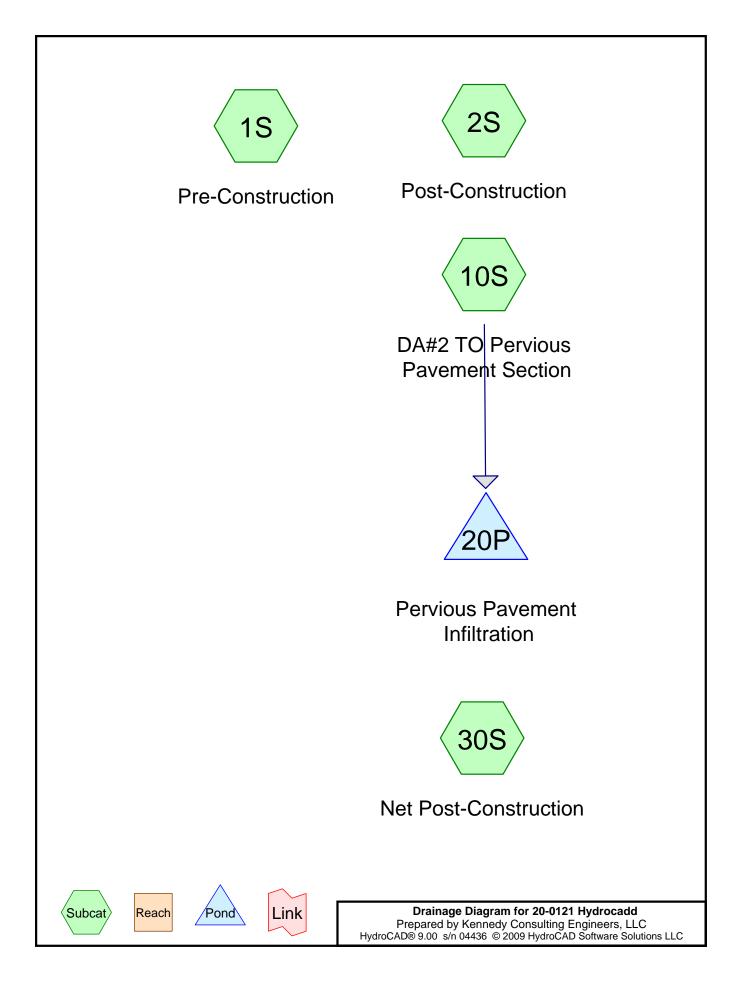
SITE SOILS, EVD: EVESBORO SAND, 10-15% SLOPES, HYDROLOGIC SOIL GROUP "A"

RUNOFF CURVE NUMBERS & DESCRIPTIONS PRE POST										
98 IMPERVIOUS SITE COVERAGE, SQ. FT.224263339 >75% GRASS COVER, GOOD CONDITION, SQ. FT.1134131736 WOODS, FAIR CONDITION, SQ. FT.9300024WEIGHTED AVERAGE CN:44										
SOILS REPORT PERMEABILITY TESTING TEST PIT SUB-SOILS 3-3.5' DEPTHS, IN/HR TP#1 TP#2 TP#3 TP#4 TP#5 AVERAGE SF DESIGN IN/HR 20 20 0.6 2.6 2 9.0 2 4.5										
PERVIOUS PAVEMENT HORIZONTAL AREA, SQ. FT.9600DESIGN INFILTRATION RATE, IN/HR4.5DESIGN INFILTRATION RATE, FPS0.0002DESIGN INFILTRATION RATE FOR PERVIOUS PAVEMENT SECTION, CFS1.0										
ENTER DEPTH OF GRAVEL BASE STORAGE SECTION, FT. ENTER VOID RATIO DESIGN STORAGE VOLUME, AREA X DEPTH X VOID RATIO, CU. FT.		1.33 0.4 5120								
DEPTH OF 100 YEAR-24 HOUR STORM STAGE IN GRAVEL BASE SECTION, FT.		1.27 OK								
COMPLIANCE DATAPREPOST2 YEAR HYDROGRAPH RUNOFF VOLUMES, CU. FT.10252012MIN. REQUIRED FOR GROUNDWATER RECHARGE, POST-PRE, CU. FT.987										
DESIGN GROUNDWATER RECHARGE PROVIDED 2 YR STORM, CU. FT. 1511 OK										

## PRE-CONSTRUCTION TO NET POST-CONSTRUCTION PEAK RATES AND VOLUMES

	PRE-CONST	RUCTION	NET POST-CONSTRUCTION			
	228,839 SQ.	FT., CN=44	164,473 SQ. FT., CN=44			
	CFS	CU. FT.	CFS	CU. FT.		
	0.04	1025	0.02			
2 YEAR STORM	0101		0.03	737 OK		
10 YEAR STORM	0.99	8736	0.76	6279 OK		
25 YEAR STORM	2.90	17877	2.50	12849 OK		
100 YEAR STORM	8.67	40355	7.60	29004 OK		





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# 20-0121 Hydrocadd

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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
141,000	36	Woods, Fair, HSG A (1S, 2S, 30S)
459,015	39	>75% Grass cover, Good, HSG A (1S, 2S, 10S, 30S)
16,022	98	(10S)
32,037	98	14% Lot Coverage (2S)
16,015	98	14% Lot Coverage less pavement (30S)
22,426	98	9.8% Lot Coverage (1S)
686,515		TOTAL AREA

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# Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
600,015	HSG A	1S, 2S, 1OS, 3OS
0	HSG B	
0	HSG C	
0	HSG D	
86,500	Other	1S, 2S, 10S, 30S
686,515		TOTAL AREA

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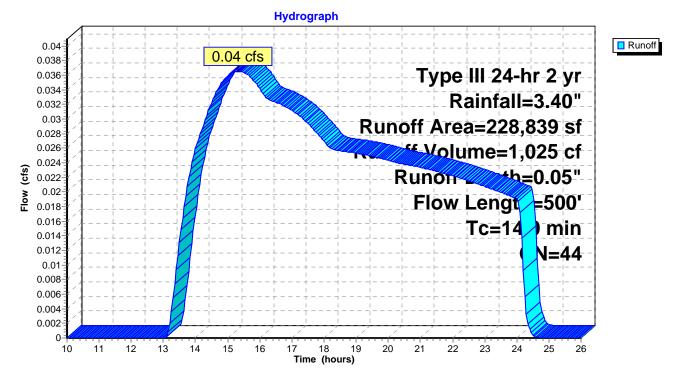
Time span=10.00-26.00 hrs, dt=0.05 hrs, 321 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method							
Subcatchment 1S: Pre-Construction	Runoff Area=228,839 sf 9.80% Impervious Runoff Depth=0.05" ow Length=500' Tc=14.0 min CN=44 Runoff=0.04 cfs 1,025 cf						
Subcatchment 2S: Post-Construction	Runoff Area=228,838 sf 14.00% Impervious Runoff Depth=0.11" ow Length=500' Tc=14.0 min CN=47 Runoff=0.08 cfs 2,012 cf						
Subcatchment 10S: DA#2 TO Pervious Pavement Flow Length=150'							
Subcatchment 30S: Net Post-Construction	Runoff Area=164,473 sf 9.74% Impervious Runoff Depth=0.05" Flow Length=290' Tc=7.5 min CN=44 Runoff=0.03 cfs 737 cf						
Pond 20P: Pervious Pavement Infiltration	Peak Elev=0.02' Storage=61 cf Inflow=0.17 cfs 1,511 cf Outflow=0.16 cfs 1,511 cf						

Total Runoff Area = 686,515 sf Runoff Volume = 5,285 cf Average Runoff Depth = 0.09" 87.40% Pervious = 600,015 sf 12.60% Impervious = 86,500 sf

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	Summary for Subcatchment 1S: Pre-Construction							
Runoff	=	0.04	cfs @ 15.	32 hrs, Volu	ume= 1,025 cf, Depth= 0.05"			
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 2 yr Rainfall=3.40"							
	Area (sf)	CN D	escription					
*	22,426	98 9	.8% Lot Co	overage				
	93,000	36 V	Voods, Faiı	, HSG A				
1	13,413	39 >	75% Gras	s cover, Go	ood, HSG A			
2	228,839	44 V	Veighted A	verage				
2	206,413	9	0.20% Per	vious Area				
	22,426	9	.80% Impe	ervious Arec	I			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
8.9	150	0.0570	0.28		Sheet Flow, Elev 122.5 to 114			
5.1	350	0.0520	1.14		Grass: Short $n = 0.150$ P2= 3.20"			
5.1		0.0520	1.14		Shallow Concentrated Flow, To Cheswick Court Woodland Kv= 5.0 fps			
14.0	500	Total						

### Subcatchment 1S: Pre-Construction



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# Hydrograph for Subcatchment 1S: Pre-Construction

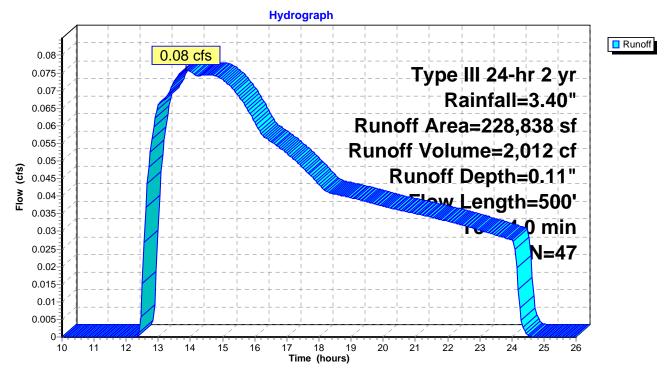
Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)		(Cfs)	(hours)	(inches)		(Cfs)
10.00	0.64	0.00	0.00	23.00	3.37	0.05	0.02
10.25	0.69	0.00	0.00	23.25	3.38	0.05	0.02
10.50	0.74	0.00	0.00	23.50	3.39	0.05	0.02
10.75	0.79	0.00	0.00	23.75	3.39	0.05	0.02
11.00	0.85	0.00	0.00	24.00	3.40	0.05	0.02
11.25	0.92	0.00	0.00	24.25	3.40	0.05	0.01
11.50	1.01	0.00	0.00	24.50	3.40	0.05	0.00
11.75	1.21	0.00	0.00	24.75	3.40	0.05	0.00
12.00	1.70	0.00	0.00	25.00	3.40	0.05	0.00
12.25	2.19	0.00	0.00	25.25	3.40	0.05	0.00
12.50	2.39	0.00	0.00	25.50	3.40	0.05	0.00
12.75	2.48	0.00	0.00	25.75	3.40	0.05	0.00
13.00 13.25	2.55 2.61	0.00 0.00	0.00 0.00	26.00	3.40	0.05	0.00
13.25	2.66	0.00	0.00				
13.75	2.00	0.00	0.02				
14.00	2.76	0.00	0.02				
14.25	2.80	0.00	0.03				
14.50	2.84	0.01	0.03				
14.75	2.87	0.01	0.03				
15.00	2.90	0.01	0.04				
15.25	2.94	0.01	0.04				
15.50	2.96	0.01	0.04				
15.75	2.99	0.01	0.04				
16.00	3.01	0.02	0.03				
16.25	3.03	0.02	0.03				
16.50	3.05	0.02	0.03				
16.75	3.07	0.02	0.03				
17.00	3.09	0.02	0.03				
17.25 17.50	3.11 3.13	0.02 0.03	0.03 0.03				
17.30	3.13	0.03	0.03				
18.00	3.16	0.03	0.03				
18.25	3.17	0.03	0.03				
18.50	3.18	0.03	0.03				
18.75	3.19	0.03	0.03				
19.00	3.21	0.03	0.03				
19.25	3.22	0.03	0.03				
19.50	3.23	0.04	0.02				
19.75	3.24	0.04	0.02				
20.00	3.25	0.04	0.02				
20.25	3.26	0.04	0.02				
20.50	3.28	0.04	0.02				
20.75	3.29	0.04	0.02				
21.00 21.25	3.30 3.31	0.04 0.04	0.02 0.02				
21.25	3.31	0.04	0.02				
21.30	3.33	0.04	0.02				
22.00	3.33	0.05	0.02				
22.25	3.34	0.05	0.02				
22.50	3.35	0.05	0.02				
22.75	3.36	0.05	0.02				

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$\begin{array}{rcl} {\sf Runoff} & = & 0.08 \ {\sf cfs} @ & 13.87 \ {\sf hrs}, \ {\sf Volume} = & 2,012 \ {\sf cf}, \ {\sf Depth} = \ 0.11" \\ {\sf Runoff} \ {\sf by} \ {\sf SCS} \ {\sf TR-20} \ {\sf method}, \ {\sf UH} = {\sf SCS}, \ {\sf Time} \ {\sf Span} = & 10.00-26.00 \ {\sf hrs}, \ {\sf dt} = & 0.05 \ {\sf hrs} \\ {\sf Type} \ {\sf III} \ 24-{\sf hr} \ 2 \ {\sf yr} \ {\sf Rainfall} = & 3.40" \\ \\ \hline $								
Type III 24-hr 2 yr Rainfall=3.40"Area (sf)CNDescription* $32,037$ 9814% Lot Coverage24,00036Woods, Fair, HSG A172,80139>75% Grass cover, Good, HSG A228,83847Weighted Average196,80186.00% Pervious Area32,03714.00% Impervious AreaTc Length Slope Velocity Capacity Description(min)(feet)(ft/ft)(ft/ft)(ft/sec)(cfs)8.91500.05700.28Sheet Flow, Elev 122.5 to 114 Grass: Shortn = 0.150P2 = 3.20"	Runoff	=	0.08 cfs @ 13.87 hrs, Volume= 2,012 cf, Depth= 0.11"					
Area (sf)CNDescription* $32,037$ 98 $14\%$ Lot Coverage $24,000$ 36Woods, Fair, HSG A $172,801$ 39>75% Grass cover, Good, HSG A $228,838$ 47Weighted Average $196,801$ $86.00\%$ Pervious Area $32,037$ $14.00\%$ Impervious AreaTcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/ft)(ft/sec)(cfs)8.91500.05700.28Sheet Flow, Elev 122.5 to 114Grass: ShortGrass: Shortn= 0.150P2= $3.20"$		•						
*       32,037       98       14% Lot Coverage         24,000       36       Woods, Fair, HSG A         172,801       39       >75% Grass cover, Good, HSG A         228,838       47       Weighted Average         196,801       86.00% Pervious Area         32,037       14.00% Impervious Area         Tc       Length       Slope       Velocity       Capacity       Description         (min)       (feet)       (ft/ft)       (ft/sec)       (cfs)         8.9       150       0.0570       0.28       Sheet Flow, Elev 122.5 to 114         Grass: Short       n = 0.150       P2= 3.20"	Type III 2	24-hr 2 yr	r Rainfall=3.40"					
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	/	Area (sf)	CN Description					
172,801       39       >75% Grass cover, Good, HSG A         228,838       47       Weighted Average         196,801       86.00% Pervious Area         32,037       14.00% Impervious Area         Tc       Length       Slope       Velocity       Capacity       Description         (min)       (feet)       (ff/ft)       (ff/sec)       (cfs)         8.9       150       0.0570       0.28       Sheet Flow, Elev 122.5 to 114         Grass:       Short       n = 0.150       P2 = 3.20"	*	32,037	98 14% Lot Coverage					
228,838       47       Weighted Average         196,801       86.00% Pervious Area         32,037       14.00% Impervious Area         Tc       Length       Slope       Velocity       Capacity       Description         (min)       (feet)       (ft/ft)       (ft/sec)       (cfs)         8.9       150       0.0570       0.28       Sheet Flow, Elev 122.5 to 114         Grass:       Short       n=       0.150       P2=       3.20"		24,000	36 Woods, Fair, HSG A					
196,801       86.00% Pervious Area         32,037       14.00% Impervious Area         Tc       Length       Slope       Velocity       Capacity       Description         (min)       (feet)       (ft/ft)       (ft/sec)       (cfs)         8.9       150       0.0570       0.28       Sheet Flow, Elev 122.5 to 114         Grass:       Short       n = 0.150       P2 = 3.20"		172,801	39 >75% Grass cover, Good, HSG A					
32,037       14.00% Impervious Area         Tc       Length       Slope       Velocity       Capacity       Description         (min)       (feet)       (ff/ft)       (ff/sec)       (cfs)         8.9       150       0.0570       0.28       Sheet Flow, Elev 122.5 to 114 Grass: Short       n= 0.150       P2= 3.20"		228,838 47 Weighted Average						
TcLengthSlopeVelocityCapacityDescription(min)(feet)(ff/ft)(ff/sec)(cfs) $8.9$ 1500.05700.28Sheet Flow, Elev 122.5 to 114 Grass: Shortn= 0.150P2= 3.20"	Ī	• •						
(min)         (feet)         (ff/ft)         (ff/sec)         (cfs)           8.9         150         0.0570         0.28         Sheet Flow, Elev 122.5 to 114           Grass:         Short         n = 0.150         P2 = 3.20"		32,037	14.00% Impervious Area					
(min)         (feet)         (ff/ft)         (ff/sec)         (cfs)           8.9         150         0.0570         0.28         Sheet Flow, Elev 122.5 to 114           Grass:         Short         n = 0.150         P2 = 3.20"								
8.9         150         0.0570         0.28         Sheet Flow, Elev 122.5 to 114           Grass: Short         n = 0.150         P2 = 3.20"	Tc	Length	Slope Velocity Capacity Description					
Grass: Short n = 0.150 P2= 3.20"	(min)	(feet)	(ft/ft) (ft/sec) (cfs)					
	8.9	150	0.0570 0.28 Sheet Flow, Elev 122.5 to 114					
5.1 350 0.0520 1.14 Shallow Concentrated Flow, To Cheswick Court			Grass: Short n= 0.150 P2= 3.20"					
	5.1	350	0.0520 1.14 Shallow Concentrated Flow, To Cheswick	Court				
Woodland Kv= 5.0 fps			Woodland Kv= 5.0 fps					
14.0 500 Total	14.0	500	Total					

Summary for Subcatchment 2S: Post-Construction

## Subcatchment 2S: Post-Construction



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# Hydrograph for Subcatchment 2S: Post-Construction

Time         Precip.         Excess         Runoff           [hours]         (inches)         (inches)         (inches)         (inches)         (inches)           10.00         0.44         0.00         0.00         23.25         3.38         0.10         0.03           10.50         0.74         0.00         0.00         23.25         3.39         0.10         0.03           10.75         0.79         0.00         0.00         23.25         3.39         0.10         0.03           11.02         0.85         0.00         0.00         24.25         3.40         0.11         0.03           11.25         0.92         0.00         0.00         24.55         3.40         0.11         0.00           11.75         1.21         0.00         0.00         25.50         3.40         0.11         0.00           12.00         1.70         0.00         0.02         25.55         3.40         0.11         0.00           12.05         2.48         0.00         0.05         25.75         3.40         0.11         0.00           13.25         2.60         0.02         0.07         13.75         2.71         0.02         0.0			_				_	
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11.00       0.85       0.00       0.00       24.00       3.40       0.11       0.03         11.25       0.92       0.00       0.00       24.55       3.40       0.11       0.00         11.75       1.21       0.00       0.00       24.50       3.40       0.11       0.00         12.00       1.70       0.00       0.00       24.55       3.40       0.11       0.00         12.25       2.19       0.00       0.00       25.25       3.40       0.11       0.00         12.50       2.39       0.00       0.02       25.55       3.40       0.11       0.00         13.00       2.55       0.11       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       15.55       2.94       0.04       0.07       15.55       2.94       0.04       0.07       15.55       2.94       0.04       0.07       15.55       2.94       0.04       0.07       15.55       2.99       0.44       0.07       16.00       3.05       0.66       16.55 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>								
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11.75       1.21       0.00       0.00       24.75       3.40       0.11       0.00         12.00       1.70       0.00       0.00       25.00       3.40       0.11       0.00         12.25       2.19       0.00       0.02       25.25       3.40       0.11       0.00         12.50       2.39       0.00       0.02       25.55       3.40       0.11       0.00         12.55       2.48       0.00       0.05       25.75       3.40       0.11       0.00         13.25       2.61       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       26.00       3.40       0.11       0.00         13.55       2.61       0.01       0.07       26.00       3.40       0.11       0.00         14.25       2.80       0.02       0.07       14.50       2.84       0.03       0.07         14.50       2.84       0.03       0.07       15.50       2.99       0.04       0.07         15.50       2.96       0.04       0.07       16.00       3.01       0.05       0.06         16.50       3.0								
12.00       1.70       0.00       0.00       25.00       3.40       0.11       0.00         12.25       2.19       0.00       0.00       25.25       3.40       0.11       0.00         12.50       2.39       0.00       0.02       25.50       3.40       0.11       0.00         12.75       2.48       0.00       0.07       26.00       3.40       0.11       0.00         13.00       2.55       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       0.3.40       0.11       0.00         14.75       2.87       0.03       0.07       0.4       0.07       15.50       2.96       0.04       0.07         15.50       2.96       0.04       0.07       15.50       2.96       0.04       0.07         15.50       2.96       0.04       0.07       15.50       3.03       0.05       0.06         16.25       3.03       0.05       0.06       16.55       3.13       0.06       0.05         17.2								
12.25       2.19       0.00       0.00       25.25       3.40       0.11       0.00         12.50       2.39       0.00       0.05       25.75       3.40       0.11       0.00         13.00       2.55       0.01       0.07       26.00       3.40       0.11       0.00         13.25       2.61       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       26.00       3.40       0.11       0.00         14.00       2.76       0.02       0.08       14.42       2.80       0.02       0.07         14.55       2.87       0.03       0.07       15.50       2.99       0.04       0.07         15.50       2.90       0.04       0.07       15.55       2.99       0.04       0.07         15.55       2.99       0.04       0.07       15.50       3.05       0.06       16.55       3.03       0.05       1.4								
12.50       2.39       0.00       0.02       25.50       3.40       0.11       0.00         13.00       2.55       0.01       0.07       26.00       3.40       0.11       0.00         13.25       2.61       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.01       0.07       26.00       3.40       0.11       0.00         13.50       2.66       0.02       0.08       0.11       0.00         14.50       2.84       0.03       0.07       0.45       0.4       0.07         14.50       2.84       0.03       0.07       0.50       2.96       0.04       0.07         15.50       2.96       0.04       0.07       0.50       0.66       0.65       0.65       0.66       0.65       0.66       0.65       0.66       0.65       0.75       0.40       0.07       0.64       0.05       0.64       0.65       0.65       0.66       0.65       0.66       0.65       0.66       0.65       0.75       0.41       0.60       0.5       0.64       0.55       0.64       0.65       0.64       0.65       0.64       0.65       0.64								
12.75       2.48       0.00       0.05       25.75       3.40       0.11       0.00         13.00       2.55       0.01       0.07       26.00       3.40       0.11       0.00         13.25       2.61       0.01       0.07       26.00       3.40       0.11       0.00         13.75       2.71       0.02       0.08       0.14.00       2.76       0.02       0.08         14.25       2.80       0.02       0.07       0.14.75       2.87       0.03       0.07         14.50       2.84       0.03       0.07       0.15.00       2.90       0.04       0.07         15.50       2.94       0.04       0.07       0.55       0.06       0.66         16.25       3.03       0.05       0.06       0.05       0.75       0.40       0.07         15.60       2.99       0.04       0.07       0.66       0.05       0.75       0.66       0.65         17.00       3.09       0.06       0.05       0.75       0.41       0.25       0.77       0.04         18.00       3.16       0.07       0.04       0.85       0.41       0.75       0.22       0.88       0.								
13.00       2.55       0.01       0.07       26.00       3.40       0.11       0.00         13.25       2.61       0.01       0.07       0.08       0.11       0.00         13.50       2.66       0.01       0.07       0.08       0.11       0.00         14.00       2.76       0.02       0.08       0.11       0.00         14.25       2.80       0.02       0.07       0.14       0.07       0.03       0.07         14.50       2.84       0.03       0.07       0.50       2.90       0.04       0.07         15.00       2.90       0.04       0.07       0.50       0.66       0.65         15.50       2.96       0.04       0.07       0.66       0.65       0.64       0.67         16.00       3.01       0.05       0.06       0.05       0.66       0.05       0.66       0.05       0.66       0.05       0.75       0.75       0.13       0.06       0.05       0.75       0.75       0.14       0.60       0.5       0.75       0.75       0.75       0.75       0.75       0.75       0.83       0.04       0.75       0.75       0.83       0.04       0.75								
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14.00       2.76       0.02       0.07         14.25       2.80       0.02       0.07         14.50       2.84       0.03       0.07         14.75       2.87       0.03       0.07         15.00       2.90       0.04       0.07         15.55       2.94       0.04       0.07         15.50       2.96       0.04       0.07         16.00       3.01       0.05       0.06         16.25       3.03       0.05       0.06         16.50       3.05       0.05       0.06         16.75       3.07       0.06       0.05         17.00       3.09       0.06       0.05         17.75       3.11       0.06       0.05         17.75       3.14       0.06       0.05         17.75       3.14       0.06       0.05         18.00       3.16       0.07       0.04         18.75       3.19       0.07       0.04         18.75       3.19       0.07       0.04         19.05       3.23       0.08       0.04         20.00       3.25       0.08       0.04      19.05       3.24<								
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20.50       3.28       0.08       0.04         20.75       3.29       0.09       0.04         21.00       3.30       0.09       0.04         21.25       3.31       0.09       0.03         21.50       3.32       0.09       0.03         21.75       3.33       0.09       0.03         22.00       3.33       0.09       0.03         22.25       3.34       0.10       0.03         22.50       3.35       0.10       0.03								
20.753.290.090.0421.003.300.090.0421.253.310.090.0321.503.320.090.0321.753.330.090.0322.003.330.090.0322.253.340.100.0322.503.350.100.03								
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21.753.330.090.0322.003.330.090.0322.253.340.100.0322.503.350.100.03								
22.00       3.33       0.09       0.03         22.25       3.34       0.10       0.03         22.50       3.35       0.10       0.03								
22.25         3.34         0.10         0.03           22.50         3.35         0.10         0.03								
22.50 3.35 0.10 0.03								
22.75 3.30 0.10 0.03								
	22.75	3.30	0.10	0.03	I			

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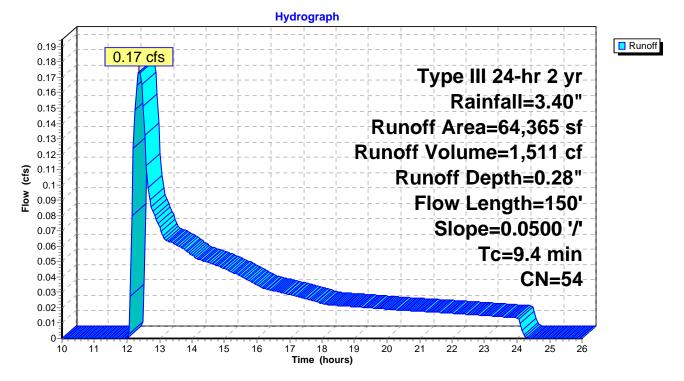
#### Summary for Subcatchment 10S: DA#2 TO Pervious Pavement Section

Runoff = 0.17 cfs @ 12.37 hrs, Volume = 1,511 cf, Depth = 0.28"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 2 yr Rainfall= $3.40^{\circ}$ 

_	ŀ	Area (sf)	CN	Description		
*		16,022	98			
_		48,343	39	>75% Gras	s cover, Go	od, HSG A
		64,365	54	Weighted A	verage	
		48,343		75.11% Per	vious Area	
		16,022		24.89% Imp	pervious Are	a
	Tc	Length	Slop	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/f	t) (ft/sec)	(Cfs)	
	9.4	150	0.050	0 0.27		Sheet Flow, ELEV. 122.5 TO 115
						Grass: Short n = 0.150 P2= 3.20"

#### Subcatchment 10S: DA#2 TO Pervious Pavement Section



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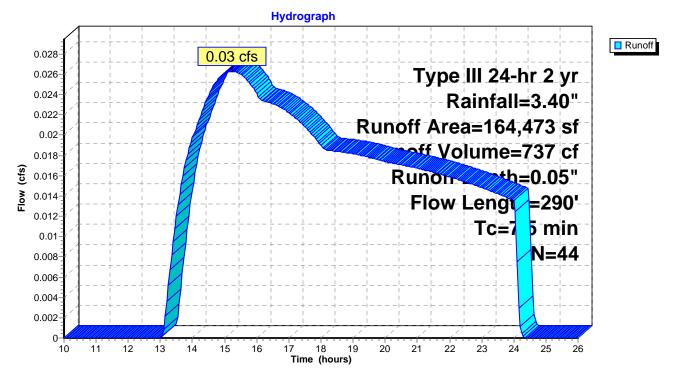
# Hydrograph for Subcatchment 10S: DA#2 TO Pervious Pavement Section

Time	Dragin	Even	Dunoff	Time	Dragin	Even	Dupoff
Time (hours)	Precip. (inches)		Runoff (cfs)	Time (hours)	Precip.	Excess (inches)	Runoff (cfs)
10.00	0.64	0.00	0.00	23.00	<u>(incries)</u> 3.37	0.27	0.01
10.00	0.69	0.00	0.00	23.25	3.38	0.27	0.01
10.20	0.74	0.00	0.00	23.50	3.39	0.28	0.01
10.75	0.79	0.00	0.00	23.75	3.39	0.28	0.01
11.00	0.85	0.00	0.00	24.00	3.40	0.28	0.01
11.25	0.92	0.00	0.00	24.25	3.40	0.28	0.00
11.50	1.01	0.00	0.00	24.50	3.40	0.28	0.00
11.75	1.21	0.00	0.00	24.75	3.40	0.28	0.00
12.00	1.70	0.00	0.00	25.00	3.40	0.28	0.00
12.25	2.19	0.03	0.15	25.25	3.40	0.28	0.00
12.50	2.39	0.05	0.15	25.50	3.40	0.28	0.00
12.75	2.48	0.06	0.09	25.75	3.40	0.28	0.00
13.00	2.55	0.08	0.07	26.00	3.40	0.28	0.00
13.25	2.61	0.09	0.06				
13.50	2.66	0.10	0.06				
13.75	2.71	0.11	0.06				
14.00	2.76	0.12	0.05				
14.25	2.80	0.12	0.05				
14.50	2.84	0.13	0.05				
14.75	2.87	0.14	0.05				
15.00	2.90	0.15	0.05				
15.25	2.94	0.16	0.04				
15.50	2.96	0.16	0.04				
15.75	2.99	0.17	0.04				
16.00	3.01	0.17	0.03 0.03				
16.25 16.50	3.03 3.05	0.18 0.18	0.03				
16.75	3.03	0.10	0.03				
17.00	3.09	0.19	0.03				
17.25	3.11	0.20	0.03				
17.50	3.13	0.20	0.03				
17.75	3.14	0.21	0.02				
18.00	3.16	0.21	0.02				
18.25	3.17	0.21	0.02				
18.50	3.18	0.22	0.02				
18.75	3.19	0.22	0.02				
19.00	3.21	0.23	0.02				
19.25	3.22	0.23	0.02				
19.50	3.23	0.23	0.02				
19.75	3.24	0.24	0.02				
20.00	3.25	0.24	0.02				
20.25	3.26	0.24	0.02				
20.50	3.28	0.24	0.02				
20.75	3.29	0.25	0.02				
21.00	3.30	0.25	0.02				
21.25	3.31 3.32	0.25	0.02				
21.50 21.75	3.32	0.26 0.26	0.02 0.02				
21.75	3.33	0.26	0.02				
22.00	3.33	0.26	0.02				
22.25	3.35	0.20	0.02				
22.30	3.36	0.27	0.02				
0	5,00	512/	0.02	l			

		<b>5</b> u	mmary i	or subcaid	chment 305: Net Post-Construction			
Runoff	=	0.03 0	cfs @ 15.	22 hrs, Volu	ume= 737 cf, Depth= 0.05"			
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 2 yr Rainfall=3.40"							
	Area (sf)	CN D	escription					
*	16,015	98 1	4% Lot Co	verage less	pavement			
	24,000	36 V	loods, Fai	r, HSG A				
	124,458	39 >	75% Gras	s cover, Go	ood, HSG A			
	164,473	44 V	/eighted A	verage				
	148,458	9	0.26% Per	vious Area				
	16,015	9	.74% Impe	ervious Arec	1			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(Cfs)				
4.8	66	0.0530	0.23		Sheet Flow, Elev 116 to 112.5			
					Grass: Short n= 0.150 P2= 3.20"			
2.7	224	0.0750	1.37		Shallow Concentrated Flow, To Cheswick Court			
					Woodland Kv= 5.0 fps			
7.5	290	Total						

## Summary for Subcatchment 30S: Net Post-Construction

#### Subcatchment 30S: Net Post-Construction



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# Hydrograph for Subcatchment 30S: Net Post-Construction

	<b>_</b> .	_		·	<b>_</b> .	_	- "
Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)	(inches)	(cfs)
10.00	0.64	0.00	0.00	23.00	3.37	0.05	0.01
10.25	0.69	0.00	0.00	23.25	3.38	0.05	0.01
10.50	0.74	0.00	0.00	23.50	3.39	0.05	0.01
10.75	0.79	0.00	0.00	23.75	3.39	0.05	0.01
11.00	0.85	0.00	0.00	24.00	3.40	0.05	0.01
11.25	0.92	0.00	0.00	24.25	3.40	0.05	0.00
11.50	1.01	0.00	0.00	24.50	3.40	0.05	0.00
11.75	1.21	0.00	0.00	24.75	3.40	0.05	0.00
12.00	1.70	0.00	0.00	25.00	3.40	0.05	0.00
12.25	2.19	0.00	0.00	25.25	3.40	0.05	0.00
12.50	2.39	0.00	0.00	25.50	3.40	0.05	0.00
12.75	2.48	0.00	0.00	25.75	3.40	0.05	0.00
13.00	2.55	0.00	0.00	26.00	3.40	0.05	0.00
13.25	2.61	0.00	0.01				
13.50	2.66	0.00	0.01				
13.75	2.71	0.00	0.02				
14.00	2.76	0.00	0.02				
14.25	2.80	0.00	0.02				
14.50	2.84	0.01	0.02				
14.75	2.87	0.01	0.03				
15.00	2.90	0.01	0.03				
15.25	2.94	0.01	0.03				
15.50	2.96	0.01	0.03				
15.75	2.99	0.01	0.03				
16.00	3.01	0.02	0.02				
16.25	3.03	0.02	0.02				
16.50	3.05	0.02	0.02				
16.75	3.07	0.02	0.02				
17.00	3.09	0.02	0.02				
17.25	3.11	0.02	0.02				
17.50	3.13	0.03	0.02				
17.75	3.14	0.03	0.02				
18.00	3.16	0.03	0.02				
18.25	3.17	0.03	0.02				
18.50	3.18	0.03	0.02				
18.75	3.19	0.03	0.02				
19.00	3.21	0.03	0.02				
19.25	3.22	0.03	0.02				
19.50	3.23	0.04	0.02				
19.75	3.24	0.04	0.02				
20.00	3.25	0.04	0.02				
20.25	3.26	0.04	0.02				
20.50	3.28	0.04	0.02				
20.75	3.29	0.04	0.02				
21.00	3.30	0.04	0.02				
21.25	3.31	0.04	0.02				
21.50	3.32	0.04	0.02				
21.75	3.33	0.05	0.02				
22.00	3.33	0.05	0.02				
22.25	3.34	0.05	0.02				
22.50	3.35	0.05	0.02				
22.75	3.36	0.05	0.02				

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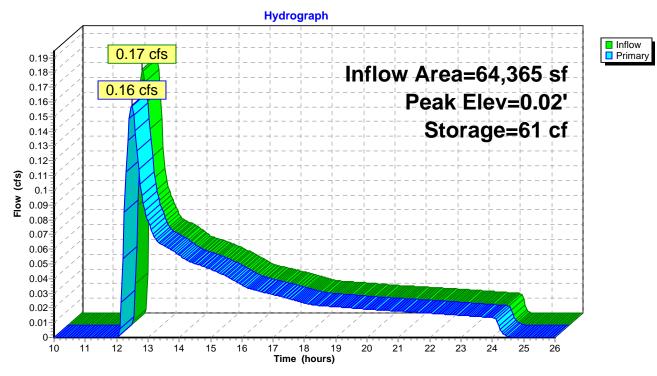
## Summary for Pond 20P: Pervious Pavement Infiltration

Inflow Area =       64,365 sf, 24.89% Impervious, Inflow Depth =       0.28" for 2 yr event         Inflow =       0.17 cfs @       12.37 hrs, Volume=       1,511 cf         Outflow =       0.16 cfs @       12.48 hrs, Volume=       1,511 cf, Atten= 9%, Lag= 6.4 min         Primary =       0.16 cfs @       12.48 hrs, Volume=       1,511 cf						
Routing by Stor-Ind method, Time Span= $10.00-26.00$ hrs, dt= 0.05 hrs						
Peak Elev= 0.02' @ 12.48 hrs Surf.Area= 0 sf Storage= 61 cf						
Plug-Flow detention time = 6.4 min calculated for 1,506 cf (100% of inflow) Center-of-Mass det. time = 6.4 min ( 960.8 - 954.4 )						
Volume Invert Avail.Storage Storage Description						
#1 0.00' 5,120 cf Custom Stage Data Listed below						
Elevation Cum.Store (feet) (cubic-feet)						
0.00 0						
1.33 5,120						
Device Routing Invert Outlet Devices						
#1 Primary 0.00' 9600 sq. ft. INFILTRATION						
Elev. (feet) 0.00 0.10 1.00						
Disch. (cfs) 0.000 1.000 1.000						
Primary OutFlow Max=0.16 cfs @ 12.48 hrs HW=0.02' (Free Discharge)						

-1=9600 sq. ft. INFILTRATION (Custom Controls 0.16 cfs)

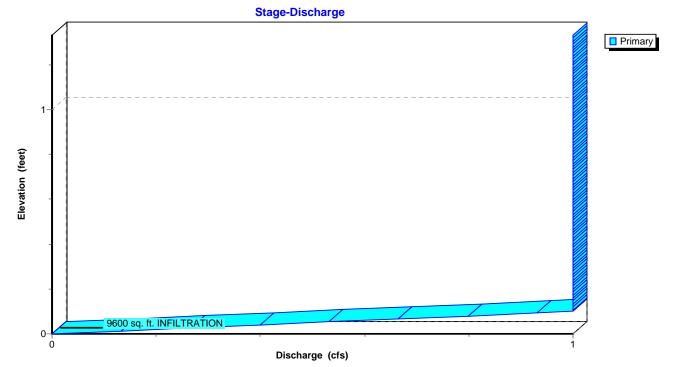
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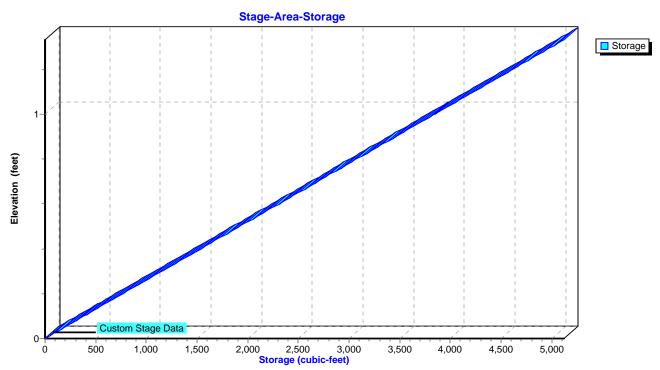




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#### Pond 20P: Pervious Pavement Infiltration

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# Hydrograph for Pond 20P: Pervious Pavement Infiltration

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(Cfs)
10.00	0.00	0	0.00	0.00
10.50	0.00	0	0.00	0.00
11.00	0.00	0	0.00	0.00
11.50	0.00	0	0.00	0.00
12.00	0.00	0	0.00	0.00
12.50	0.15	60	0.02	0.16
13.00	0.07	30	0.01	0.08
13.50	0.06	24	0.01	0.06
14.00	0.05	21	0.01	0.06
14.50	0.05	19	0.01	0.05
15.00	0.05	18	0.00	0.05
15.50	0.04	16	0.00	0.04
16.00	0.03	14	0.00	0.04
16.50	0.03	12	0.00	0.03
17.00	0.03	11	0.00	0.03
17.50	0.03	10	0.00	0.03
18.00	0.02	9	0.00	0.02
18.50	0.02	8	0.00	0.02
19.00	0.02	8	0.00	0.02
19.50	0.02	8	0.00	0.02
20.00	0.02	7	0.00	0.02
20.50	0.02	7	0.00	0.02
21.00	0.02	7	0.00	0.02
21.50	0.02	7	0.00	0.02
22.00	0.02	6	0.00	0.02
22.50	0.02	6	0.00	0.02
23.00	0.01	6	0.00	0.02
23.50	0.01	5	0.00	0.01
24.00	0.01	5	0.00	0.01
24.50	0.00	0	0.00	0.00
25.00	0.00	0	0.00	0.00
25.50	0.00	0	0.00	0.00
26.00	0.00	0	0.00	0.00

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# Stage-Discharge for Pond 20P: Pervious Pavement Infiltration

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Elevation	Primary	Elevation	Primary	Elevation	Primary
0.01         0.10         0.53         1.00         1.05         1.00           0.02         0.20         0.54         1.00         1.06         1.00           0.03         0.30         0.55         1.00         1.07         1.00           0.04         0.40         0.56         1.00         1.07         1.00           0.05         0.50         0.57         1.00         1.09         1.00           0.06         0.60         0.58         1.00         1.11         1.00           0.07         0.70         0.59         1.00         1.13         1.00           0.09         0.90         0.61         1.00         1.13         1.00           0.10         1.00         0.62         1.00         1.14         1.00           0.12         1.00         0.64         1.00         1.16         1.00           0.13         1.00         0.67         1.00         1.19         1.00           0.16         1.00         0.68         1.00         1.22         1.00           0.16         1.00         0.67         1.00         1.21         1.00           0.16         1.00         0.71	(feet)	(cfs)				
0.02         0.20         0.54         1.00         1.06         1.00           0.04         0.40         0.55         1.00         1.07         1.00           0.05         0.50         0.57         1.00         1.09         1.00           0.06         0.60         0.58         1.00         1.11         1.00           0.07         0.70         0.59         1.00         1.11         1.00           0.08         0.80         0.60         1.00         1.13         1.00           0.10         1.00         0.62         1.00         1.14         1.00           0.11         1.00         0.64         1.00         1.16         1.00           0.11         1.00         0.64         1.00         1.16         1.00           0.14         1.00         0.66         1.00         1.18         1.00           0.15         1.00         0.67         1.00         1.21         1.00           0.16         1.00         0.67         1.00         1.21         1.00           0.16         1.00         0.71         1.00         1.21         1.00           0.16         1.00         0.73						
0.03         0.30         0.55         1.00         1.07         1.00           0.04         0.40         0.56         1.00         1.09         1.00           0.05         0.50         0.57         1.00         1.09         1.00           0.06         0.60         0.58         1.00         1.11         1.00           0.07         0.70         0.59         1.00         1.11         1.00           0.09         0.90         0.61         1.00         1.13         1.00           0.10         1.00         0.62         1.00         1.14         1.00           0.12         1.00         0.64         1.00         1.16         1.00           0.13         1.00         0.66         1.00         1.18         1.00           0.16         1.00         0.66         1.00         1.21         1.00           0.16         1.00         0.69         1.00         1.22         1.00           0.16         1.00         0.72         1.00         1.22         1.00           0.16         1.00         0.73         1.00         1.23         1.00           0.20         1.00         0.74						
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0.06         0.60         0.58         1.00         1.10         1.00           0.07         0.70         0.59         1.00         1.11         1.00           0.08         0.60         1.00         1.12         1.00           0.09         0.90         0.61         1.00         1.13         1.00           0.10         1.00         0.62         1.00         1.14         1.00           0.12         1.00         0.64         1.00         1.16         1.00           0.13         1.00         0.65         1.00         1.17         1.00           0.14         1.00         0.66         1.00         1.18         1.00           0.16         1.00         0.67         1.00         1.20         1.00           0.16         1.00         0.67         1.00         1.21         1.00           0.16         1.00         0.70         1.00         1.22         1.00           0.19         1.00         0.71         1.00         1.23         1.00           0.21         1.00         0.73         1.00         1.24         1.00           0.22         1.00         0.75         1.00						
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0.09         0.90         0.61         1.00         1.13         1.00           0.10         1.00         0.62         1.00         1.14         1.00           0.11         1.00         0.63         1.00         1.16         1.00           0.12         1.00         0.64         1.00         1.16         1.00           0.13         1.00         0.66         1.00         1.17         1.00           0.14         1.00         0.66         1.00         1.19         1.00           0.16         1.00         0.67         1.00         1.19         1.00           0.16         1.00         0.69         1.00         1.21         1.00           0.17         1.00         0.71         1.00         1.23         1.00           0.20         1.00         0.73         1.00         1.24         1.00           0.21         1.00         0.75         1.00         1.27         1.00           0.23         1.00         0.76         1.00         1.28         1.00           0.24         1.00         0.76         1.00         1.31         1.00           0.25         1.00         0.77						
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	0.31		0.83			
		1.00				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.33	1.00	0.85	1.00		
	0.34	1.00	0.86	1.00		
	0.35	1.00	0.87	1.00		
	0.36	1.00	0.88			
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	0.01	1.00	1.03	1.00	l	

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# Stage-Area-Storage for Pond 20P: Pervious Pavement Infiltration

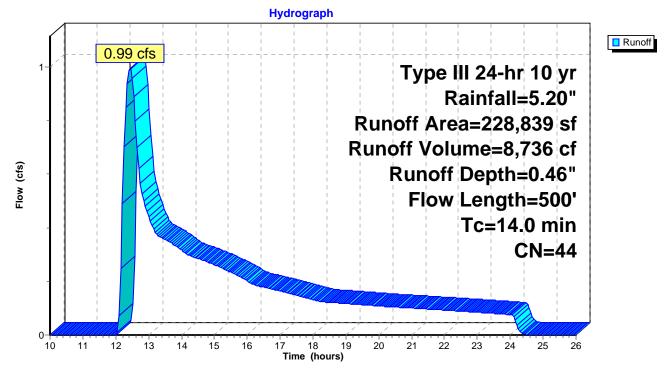
Elevation	Storage	Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)	(feet)	(cubic-feet)
0.00	0	0.52	2,002	1.04	4,004
0.00	38	0.53	2,040	1.05	4,004
0.02	77	0.54	2,040	1.06	4,042
0.02	115	0.55	2,117	1.07	4,001
0.04	154	0.56	2,156	1.08	4,158
0.05	192	0.57	2,194	1.00	4,196
0.06	231	0.58	2,134	1.10	4,170
0.07	269	0.59	2,200	1.11	4,200
0.08	308	0.60	2,310	1.12	4,273
0.09	346	0.61	2,348	1.12	4,350
0.10	385	0.62	2,387	1.14	4,389
0.11	423	0.63	2,425	1.15	4,427
0.12	462	0.64	2,464	1.16	4,466
0.13	500	0.65	2,502	1.17	4,504
0.14	539	0.66	2,541	1.18	4,543
0.15	577	0.67	2,579	1.19	4,581
0.16	616	0.68	2,618	1.20	4,620
0.17	654	0.69	2,656	1.21	4,658
0.18	693	0.70	2,695	1.22	4,697
0.19	731	0.71	2,733	1.23	4,735
0.20	770	0.72	2,772	1.24	4,774
0.21	808	0.73	2,810	1.25	4,812
0.22	847	0.74	2,849	1.26	4,851
0.23	885	0.75	2,887	1.27	4,889
0.24	924	0.76	2,926	1.28	4,928
0.25	962	0.77	2,964	1.29	4,966
0.26	1,001	0.78	3,003	1.30	5,005
0.27	1,039	0.79	3,041	1.31	5,043
0.28	1,078	0.80	3,080	1.32	5,082
0.29	1,116	0.81	3,118	1.33	5,120
0.30	1,155	0.82	3,157		
0.31	1,193	0.83	3,195		
0.32	1,232	0.84	3,234		
0.33	1,270	0.85	3,272		
0.34	1,309	0.86	3,311		
0.35	1,347	0.87	3,349		
0.36	1,386	0.88	3,388		
0.37	1,424	0.89	3,426		
0.38	1,463	0.90	3,465		
0.39	1,501	0.91	3,503		
0.40	1,540	0.92	3,542		
0.41	1,578	0.93	3,580		
0.42	1,617	0.94	3,619		
0.43	1,655	0.95	3,657		
0.44	1,694	0.96	3,696		
0.45	1,732	0.97	3,734		
0.46	1,771	0.98	3,773		
0.47	1,809	0.99	3,811		
0.48	1,848	1.00	3,850		
0.49	1,886	1.01	3,888		
0.50	1,925	1.02	3,927		
0.51	1,963	1.03	3,965		

•	0.00 hrs, dt=0.05 hrs, 32	•				
Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method						
ment 15: Bre-Construction	Pupoff Area-228 839 sf		Punoff Denth			

Subcatchment 1S: Pre-Construction	Runoff Area=228,839 sf 9.80% Impervious Runoff Depth=0.46" Flow Length=500' Tc=14.0 min CN=44 Runoff=0.99 cfs 8,736 cf
Subcatchment 2S: Post-Construction	Runoff Area=228,838 sf 14.00% Impervious Runoff Depth=0.61" ow Length=500' Tc=14.0 min CN=47 Runoff=1.61 cfs 11,627 cf
Subcatchment 10S: DA#2 TO Pervious Pavemer Flow Length=150	
Subcatchment 30S: Net Post-Construction	Runoff Area=164,473 sf 9.74% Impervious Runoff Depth=0.46" Flow Length=290' Tc=7.5 min CN=44 Runoff=0.76 cfs 6,279 cf
Pond 20P: Pervious Pavement Infiltration	Peak Elev=0.10' Storage=377 cf Inflow=1.23 cfs 5,457 cf Outflow=0.98 cfs 5,457 cf
Total Runoff Area = 686,515 s	f Runoff Volume = $32,100$ cf Average Runoff Depth = $0.56$ "

87.40% Pervious = 600,015 sf 12.60% Impervious = 86,500 sf

Summary for Subcatchment 1S: Pre-Construction										
Runoff	=	0.99	cfs @ 12.	43 hrs, Volu	ume= 8,736 cf, Depth= 0.46"					
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 10 yr Rainfall=5.20"									
Type III 2	24-111 TO y	T KUIT	uii-3.20							
/	Area (sf)	CN	Description							
*	22,426	98	9.8% Lot Co	overage						
	93,000	36	Woods, Fair	, HSG A						
	113,413	39	>75% Gras	s cover, Go	ood, HSG A					
2	228,839	44	Weighted A	verage						
2	206,413		90.20% Per	vious Area						
	22,426		9.80% Impe	ervious Area	l					
Tc	Length				Description					
(min)	(feet)	(ft/ft	) (ft/sec)	(Cfs)						
8.9	150	0.0570	0.28		Sheet Flow, Elev 122.5 to 114					
					Grass: Short n= 0.150 P2= 3.20"					
5.1	350	0.0520	0 1.14		Shallow Concentrated Flow, To Cheswick Court					
					Woodland Kv= 5.0 fps					
14.0	500	Total								
Subcatchment 1S: Pre-Construction										



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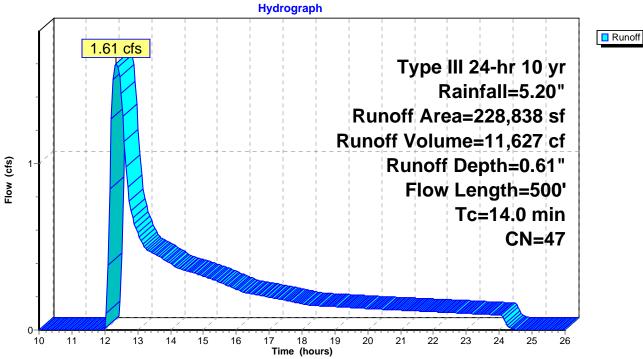
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# Hydrograph for Subcatchment 1S: Pre-Construction

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)		(cfs)
10.00	0.98	0.00	0.00	23.00	5.15	0.44	0.08
10.25	1.05	0.00	0.00	23.25	5.17	0.45	0.08
10.50	1.13	0.00	0.00	23.50	5.18	0.45	0.08
10.75	1.21	0.00	0.00	23.75	5.19	0.45	0.08
11.00	1.30	0.00	0.00	24.00	5.20	0.46	0.08
11.25	1.41	0.00	0.00	24.25	5.20	0.46	0.02
11.50	1.55	0.00	0.00	24.50	5.20	0.46	0.00
11.75 12.00	1.85 2.60	0.00 0.00	0.00 0.00	24.75 25.00	5.20 5.20	0.46 0.46	0.00 0.00
12.00	3.35	0.00	0.00 <b>0.70</b>	25.00	5.20	0.46	0.00
12.50	3.65	0.09	0.96	25.50	5.20	0.46	0.00
12.75	3.79	0.11	0.57	25.75	5.20	0.46	0.00
13.00	3.90	0.13	0.44	26.00	5.20	0.46	0.00
13.25	3.99	0.15	0.38				
13.50	4.07	0.16	0.36				
13.75	4.15	0.18	0.34				
14.00	4.22	0.19	0.32				
14.25	4.28	0.21	0.30				
14.50	4.34	0.22	0.29				
14.75	4.39	0.23	0.27				
15.00	4.44	0.25	0.26				
15.25	4.49	0.26	0.25				
15.50	4.53	0.27	0.23				
15.75 16.00	4.57 4.61	0.28 0.29	0.22 0.20				
16.25	4.64	0.29	0.20				
16.50	4.67	0.30	0.19				
16.75	4.70	0.31	0.17				
17.00	4.73	0.32	0.16				
17.25	4.76	0.33	0.16				
17.50	4.78	0.33	0.15				
17.75	4.80	0.34	0.14				
18.00	4.83	0.35	0.13				
18.25	4.85	0.35	0.12				
18.50	4.87	0.36	0.12				
18.75	4.89	0.36	0.12				
19.00	4.90	0.37	0.12				
19.25 19.50	4.92 4.94	0.37 0.38	0.11 0.11				
19.30	4.94	0.38	0.11				
20.00	4.98	0.39	0.11				
20.25	4.99	0.39	0.11				
20.50	5.01	0.40	0.10				
20.75	5.03	0.40	0.10				
21.00	5.04	0.41	0.10				
21.25	5.06	0.41	0.10				
21.50	5.07	0.42	0.10				
21.75	5.09	0.42	0.09				
22.00	5.10	0.43	0.09				
22.25	5.11	0.43	0.09				
22.50 22.75	5.13 5.14	0.44 0.44	0.09 0.09				
22.75	5.14	0.44	0.09	l			

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Summary for Subca	tchment 2S: Post-Construction
Runoff = 1.61 cfs @ 12.34 hrs, Volun	ne= 11,627 cf, Depth= 0.61"
Runoff by SCS TR-20 method, UH=SCS, Time Span Type III 24-hr 10 yr Rainfall=5.20"	ı= 10.00-26.00 hrs, dt= 0.05 hrs
Area (sf) CN Description	
* 32,037 98 14% Lot Coverage	
24,000 36 Woods, Fair, HSG A	
172,801 39 >75% Grass cover, Goo	d, HSG A
228,838 47 Weighted Average	
196,801 86.00% Pervious Area	
32,037 14.00% Impervious Area	
Tc Length Slope Velocity Capacity I (min) (feet) (ft/ft) (ft/sec) (cfs)	Description
	Sheet Flow, Elev 122.5 to 114
	Grass: Short n= 0.150 P2= 3.20"
	Shallow Concentrated Flow, To Cheswick Court
	Woodland Kv= 5.0 fps
14.0 500 Total	
Subcatchme	nt 2S: Post-Construction
Hydro	ograph
1.61 cfs	Type III 24-hr 10 yr Rainfall=5.20"
	Runoff Area=228,838 sf
	Runoff Volume=11.627 cf



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# Hydrograph for Subcatchment 2S: Post-Construction

	<b>_</b> .	_			<b>.</b> .	_	- "
Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(cfs)	(hours)	(inches)	(inches)	(cfs)
10.00	0.98	0.00	0.00	23.00	5.15	0.59	0.10
10.25	1.05	0.00	0.00	23.25	5.17	0.60	0.10
10.50	1.13	0.00	0.00	23.50	5.18	0.60	0.09
10.75	1.21	0.00	0.00	23.75	5.19	0.61	0.09
11.00	1.30	0.00	0.00	24.00	5.20	0.61	0.09
11.25	1.41	0.00	0.00	24.25	5.20	0.61	0.03
11.50	1.55	0.00	0.00	24.50	5.20	0.61	0.00
11.75	1.85	0.00	0.00	24.75	5.20	0.61	0.00
12.00	2.60	0.01	0.01	25.00	5.20	0.61	0.00
12.25	3.35	0.10	1.51	25.25	5.20	0.61	0.00
12.50	3.65	0.15	1.42	25.50	5.20	0.61	0.00
12.75	3.79	0.18	0.77	25.75	5.20	0.61	0.00
13.00	3.90	0.21	0.59	26.00	5.20	0.61	0.00
13.25	3.99	0.23	0.49				
13.50	4.07	0.25	0.46				
13.75	4.15	0.27	0.43				
14.00	4.22	0.29	0.40				
14.25	4.28	0.31	0.37				
14.50	4.34	0.32	0.36				
14.75	4.39	0.34	0.34				
15.00	4.44	0.36	0.32				
15.25	4.49	0.37	0.31				
15.50	4.53	0.38	0.29				
15.75	4.57	0.39	0.27				
16.00	4.61	0.41	0.24				
16.25	4.64	0.42	0.23				
16.50	4.67	0.43	0.22				
16.75	4.70	0.44	0.21				
17.00	4.73	0.45	0.20				
17.25	4.76	0.45	0.19				
17.50	4.78	0.46	0.18				
17.75	4.80	0.47	0.17				
18.00	4.83	0.48	0.16				
18.25	4.85	0.48	0.15				
18.50	4.87	0.49	0.15				
18.75	4.89	0.50	0.14				
19.00	4.90	0.50	0.14				
19.25	4.92	0.51	0.14				
19.50	4.94	0.52	0.13				
19.75	4.96	0.52	0.13				
20.00	4.98	0.53	0.13				
20.25	4.99	0.53	0.13				
20.50	5.01	0.54	0.12				
20.75	5.03	0.55	0.12				
21.00	5.04	0.55	0.12				
21.25	5.06	0.56	0.12				
21.50	5.07	0.56	0.11				
21.75	5.09	0.57	0.11				
22.00	5.10	0.57	0.11				
22.25	5.11	0.58	0.11				
22.50	5.13	0.58	0.10				
22.75	5.14	0.59	0.10				
				•			

#### Summary for Subcatchment 10S: DA#2 TO Pervious Pavement Section

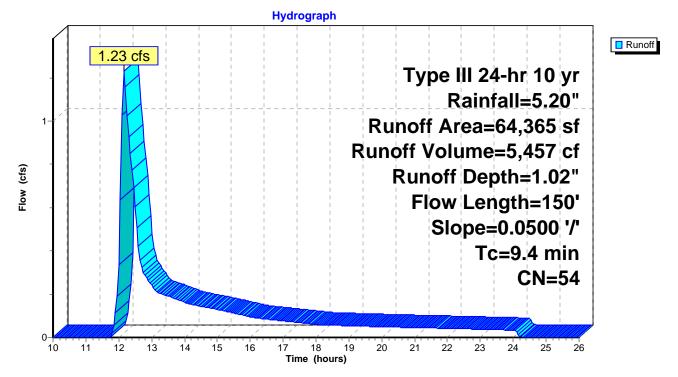
Runoff = 1.23 cfs @ 12.16 hrs, Volume = 5,457 cf, Depth = 1.02"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 10 yr Rainfall= $5.20^{\circ}$ 

	A	Area (sf)	CN	Description		
*		16,022	98			
		48,343	39	>75% Gras	s cover, Go	bod, HSG A
		64,365	54	Weighted A	verage	
		48,343		75.11% Per	vious Area	
		16,022		24.89% Imp	pervious Are	a
	Tc	Length	Slop	e Velocity	Capacity	Description
	(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
	9.4	150	0.050	0 0.27		Sheet Flow, ELEV. 122.5 TO 115

Grass: Short  $n = 0.150 P2 = 3.20^{"}$ 





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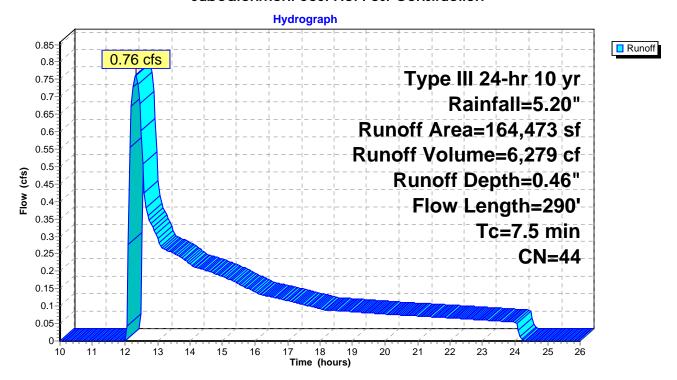
<u>Page 25</u>

# Hydrograph for Subcatchment 10S: DA#2 TO Pervious Pavement Section

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)		(Cfs)	(hours)	-		(Cfs)
10.00	0.98	0.00	0.00	23.00	5.15	0.99	0.04
10.25	1.05	0.00	0.00	23.25	5.17	1.00	0.04
10.50	1.13	0.00	0.00	23.50	5.18	1.01	0.04
10.75	1.21	0.00	0.00	23.75	5.19	1.01	0.03
11.00	1.30	0.00	0.00	24.00	5.20	1.02	0.03
11.25	1.41	0.00	0.00	24.25	5.20	1.02	0.00
11.50	1.55	0.00	0.00	24.50	5.20	1.02	0.00
11.75	1.85	0.00	0.00	24.75	5.20	1.02	0.00
12.00	2.60	0.09	0.33	25.00	5.20	1.02	0.00
12.25	3.35	0.27	1.03	25.25	5.20	1.02	0.00
12.50	3.65	0.36	0.60	25.50	5.20	1.02	0.00
12.75	3.79	0.41 0.45	0.30	25.75	5.20	1.02	0.00
13.00 13.25	3.90 3.99	0.45	0.24 0.20	26.00	5.20	1.02	0.00
13.50	4.07	0.40	0.20				
13.75	4.07	0.55	0.18				
14.00	4.10	0.57	0.16				
14.25	4.28	0.60	0.15				
14.50	4.34	0.62	0.14				
14.75	4.39	0.64	0.14				
15.00	4.44	0.67	0.13				
15.25	4.49	0.69	0.12				
15.50	4.53	0.71	0.11				
15.75	4.57	0.72	0.10				
16.00	4.61	0.74	0.09				
16.25	4.64	0.75	0.09				
16.50	4.67	0.77	0.08				
16.75	4.70	0.78	0.08				
17.00	4.73	0.79	0.08				
17.25	4.76	0.81	0.07				
17.50 17.75	4.78 4.80	0.82 0.83	0.07 0.06				
18.00	4.80	0.83	0.06				
18.25	4.85	0.85	0.06				
18.50	4.87	0.86	0.06				
18.75	4.89	0.87	0.05				
19.00	4.90	0.87	0.05				
19.25	4.92	0.88	0.05				
19.50	4.94	0.89	0.05				
19.75	4.96	0.90	0.05				
20.00	4.98	0.91	0.05				
20.25	4.99	0.92	0.05				
20.50	5.01	0.92	0.05				
20.75	5.03	0.93	0.05				
21.00	5.04	0.94	0.05				
21.25	5.06	0.95	0.04				
21.50 21.75	5.07 5.09	0.95 0.96	0.04 0.04				
21.75	5.10	0.98	0.04				
22.00	5.10	0.97	0.04				
22.20	5.13	0.98	0.04				
22.75	5.14	0.99	0.04				
				I			

	Summary for Subcatchment 30S: Net Post-Construction								
Runoff	=	0.76 c	cfs @ 12.	33 hrs, Volu	lume= 6,279 cf, Depth= 0.46"				
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 10 yr Rainfall=5.20"								
/	Area (sf)	CN D	escription						
*	16,015	98 14	4% Lot Co	verage less	ss pavement				
	24,000	36 W	loods, Fair	, HSG A					
1	24,458	39 >	75% Gras	s cover, Go	ood, HSG A				
	64,473	44 W	/eighted A	verage					
1	48,458		-	vious Area					
	16,015	9.	.74% Impe	ervious Arec	a				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•				
4.8	66	0.0530	0.23		Sheet Flow, Elev 116 to 112.5				
2.7	224	0.0750	1.37		Grass: Short n= 0.150 P2= 3.20" Shallow Concentrated Flow, To Cheswick Court				
2.7	224	0.0700	1.57		Woodland Kv= 5.0 fps				
7.5	290	Total							

### Subcatchment 30S: Net Post-Construction



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# Hydrograph for Subcatchment 30S: Net Post-Construction

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)		(Cfs)		(inches)		(Cfs)
10.00	0.98	0.00	0.00	23.00	5.15	0.44	0.06
10.25	1.05	0.00	0.00	23.25	5.17	0.45	0.06
10.50	1.13	0.00	0.00	23.50	5.18	0.45	0.06
10.75	1.21	0.00	0.00	23.75	5.19	0.45	0.06
11.00	1.30	0.00	0.00	24.00	5.20	0.46	0.05
11.25	1.41	0.00	0.00	24.25	5.20	0.46	0.00
11.50	1.55	0.00	0.00	24.50	5.20	0.46	0.00
11.75	1.85	0.00	0.00	24.75	5.20	0.46	0.00
12.00 12.25	2.60	0.00	0.00	25.00 25.25	5.20	0.46	0.00
12.25	3.35 3.65	0.05 0.09	0.73 0.60	25.25	5.20 5.20	0.46 0.46	0.00 0.00
12.30	3.79	0.11	0.35	25.75	5.20	0.46	0.00
13.00	3.90	0.13	0.33	26.00	5.20	0.46	0.00
13.25	3.99	0.15	0.26	20.00	0.20	0.40	0.00
13.50	4.07	0.16	0.25				
13.75	4.15	0.18	0.24				
14.00	4.22	0.19	0.22				
14.25	4.28	0.21	0.21				
14.50	4.34	0.22	0.20				
14.75	4.39	0.23	0.19				
15.00	4.44	0.25	0.18				
15.25	4.49	0.26	0.17				
15.50	4.53	0.27	0.16				
15.75	4.57	0.28	0.15				
16.00	4.61	0.29	0.14				
16.25	4.64	0.30	0.13				
16.50 16.75	4.67 4.70	0.30 0.31	0.13 0.12				
17.00	4.70	0.31	0.12				
17.25	4.76	0.33	0.11				
17.50	4.78	0.33	0.10				
17.75	4.80	0.34	0.10				
18.00	4.83	0.35	0.09				
18.25	4.85	0.35	0.09				
18.50	4.87	0.36	0.09				
18.75	4.89	0.36	0.09				
19.00	4.90	0.37	0.08				
19.25	4.92	0.37	0.08				
19.50	4.94	0.38	0.08				
19.75	4.96	0.38	0.08				
20.00 20.25	4.98 4.99	0.39	0.08 0.08				
20.25	4.99 5.01	0.39 0.40	0.08				
20.30	5.03	0.40	0.07				
21.00	5.04	0.40	0.07				
21.00	5.04	0.41	0.07				
21.50	5.07	0.42	0.07				
21.75	5.09	0.42	0.07				
22.00	5.10	0.43	0.07				
22.25	5.11	0.43	0.06				
22.50	5.13	0.44	0.06				
22.75	5.14	0.44	0.06				

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# Summary for Pond 20P: Pervious Pavement Infiltration

Inflow         =         1.23 cfs @           Outflow         =         0.98 cfs @	af, 24.89% Impervious, Inflow Depth = 1.02" for 10 yr event         b 12.16 hrs, Volume = 5,457 cf         c 12.28 hrs, Volume = 5,457 cf, Atten = 21%, Lag = 6.8 min         c 12.28 hrs, Volume = 5,457 cf
Routing by Stor-Ind method. Tim	ne Span= 10.00-26.00 hrs, dt= 0.05 hrs
÷ ·	Surf.Area = 0 sf Storage = 377 cf
C	Ŭ
0	min calculated for 5,440 cf (100% of inflow)
Center-of-Mass det. time= 6.4 r	min ( 902.3 - 895.9 )
Volume Invert Avail.S	Storage Storage Description
	5,120 cf <b>Custom Stage Data</b> Listed below
Elevation Cum.Store	
(feet) (cubic-feet)	
0.00 0	
1.33 5,120	

Device Routing Invert Outlet Devices	
#1 Primary 0.00' <b>9600 sq. ft. INFILTRATION</b> Elev. (feet) 0.00 0.10 1.00 Disch. (cfs) 0.000 1.000	

Primary OutFlow Max=0.98 cfs @ 12.28 hrs HW=0.10' (Free Discharge)

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#### Pond 20P: Pervious Pavement Infiltration



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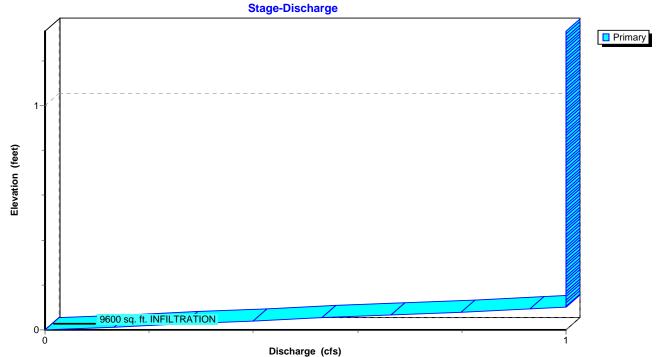
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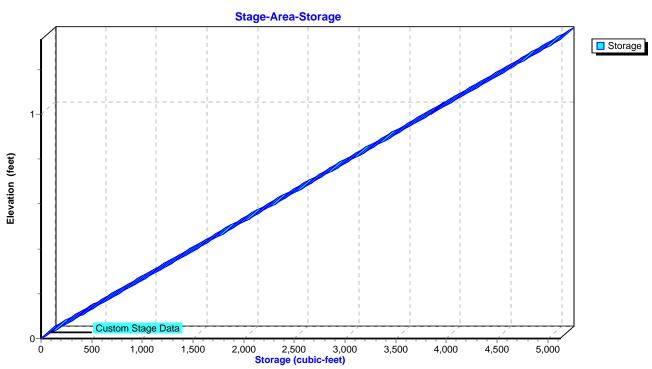
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17 18 19 Time (hours)



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#### Pond 20P: Pervious Pavement Infiltration

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# Hydrograph for Pond 20P: Pervious Pavement Infiltration

Time	Inflow	Storage	Elevation	Primary
(hours)	(Cfs)	(cubic-feet)	(feet)	(cfs)
10.00	0.00	0	0.00	0.00
10.50	0.00	0	0.00	0.00
11.00	0.00	0	0.00	0.00
11.50	0.00	0	0.00	0.00
12.00	0.33	58	0.02	0.15
12.50	0.60	294	0.08	0.76
13.00	0.24	105	0.03	0.27
13.50	0.19	76	0.02	0.20
14.00	0.16	65	0.02	0.17
14.50	0.14	57	0.01	0.15
15.00	0.13	51	0.01	0.13
15.50	0.11	45	0.01	0.12
16.00	0.09	38	0.01	0.10
16.50	0.08	33	0.01	0.09
17.00	0.08	30	0.01	0.08
17.50	0.07	27	0.01	0.07
18.00	0.06	24	0.01	0.06
18.50	0.06	22	0.01	0.06
19.00	0.05	21	0.01	0.05
19.50	0.05	20	0.01	0.05
20.00	0.05	19	0.00	0.05
20.50	0.05	18	0.00	0.05
21.00	0.05	17	0.00	0.05
21.50	0.04	17	0.00	0.04
22.00	0.04	16	0.00	0.04
22.50	0.04	15	0.00	0.04
23.00	0.04	15	0.00	0.04
23.50	0.04	14	0.00	0.04
24.00	0.03	13	0.00	0.03
24.50	0.00	1	0.00	0.00
25.00	0.00	0	0.00	0.00
25.50	0.00	0	0.00	0.00
26.00	0.00	0	0.00	0.00

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# Stage-Discharge for Pond 20P: Pervious Pavement Infiltration

Elevation	Primary	Elevation	Primary	Elevation	Primary
(feet)	(cfs)	(feet)	(cfs)	(feet)	(cfs)
0.00	0.00	0.52	1.00	1.04	1.00
0.01	0.10	0.53	1.00	1.05	1.00
0.02	0.20	0.54	1.00	1.06	1.00
0.03	0.30	0.55	1.00	1.07	1.00
0.04	0.40	0.56	1.00	1.08	1.00
0.05 0.06	0.50 0.60	0.57 0.58	1.00 1.00	1.09 1.10	1.00 1.00
0.07	0.70	0.59	1.00	1.10	1.00
0.08	0.80	0.60	1.00	1.12	1.00
0.09	0.90	0.61	1.00	1.13	1.00
0.10	1.00	0.62	1.00	1.14	1.00
0.11	1.00	0.63	1.00	1.15	1.00
0.12	1.00	0.64	1.00	1.16	1.00
0.13	1.00	0.65	1.00	1.17	1.00
0.14	1.00	0.66	1.00	1.18	1.00
0.15 0.16	1.00 1.00	0.67 0.68	1.00 1.00	1.19	1.00 1.00
0.18	1.00	0.69	1.00	1.20 1.21	1.00
0.18	1.00	0.70	1.00	1.21	1.00
0.19	1.00	0.71	1.00	1.23	1.00
0.20	1.00	0.72	1.00	1.24	1.00
0.21	1.00	0.73	1.00	1.25	1.00
0.22	1.00	0.74	1.00	1.26	1.00
0.23	1.00	0.75	1.00	1.27	1.00
0.24	1.00	0.76	1.00	1.28	1.00
0.25	1.00	0.77	1.00	1.29	1.00
0.26 0.27	1.00 1.00	0.78 0.79	1.00 1.00	1.30 1.31	1.00 1.00
0.27	1.00	0.80	1.00	1.32	1.00
0.29	1.00	0.81	1.00	1.33	1.00
0.30	1.00	0.82	1.00		
0.31	1.00	0.83	1.00		
0.32	1.00	0.84	1.00		
0.33	1.00	0.85	1.00		
0.34	1.00	0.86	1.00		
0.35 0.36	1.00 1.00	0.87 0.88	1.00 1.00		
0.30	1.00	0.88	1.00		
0.38	1.00	0.90	1.00		
0.39	1.00	0.91	1.00		
0.40	1.00	0.92	1.00		
0.41	1.00	0.93	1.00		
0.42	1.00	0.94	1.00		
0.43	1.00	0.95	1.00		
0.44	1.00	0.96	1.00		
0.45 0.46	1.00 1.00	0.97 0.98	1.00 1.00		
0.48	1.00	0.98	1.00		
0.48	1.00	1.00	1.00		
0.49	1.00	1.01	1.00		
0.50	1.00	1.02	1.00		
0.51	1.00	1.03	1.00		

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# Stage-Area-Storage for Pond 20P: Pervious Pavement Infiltration

Elevation	Storage	Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)	(feet)	(cubic-feet)
0.00	0	0.52	2,002	1.04	4,004
0.01	38	0.53	2,040	1.05	4,042
0.02	77	0.54	2,040	1.06	4,081
0.03	115	0.55	2,117	1.07	4,119
0.04	154	0.56	2,156	1.08	4,158
0.05	194	0.57	2,194	1.00	4,196
0.06	231	0.58	2,134	1.10	4,170
0.07	269	0.59	2,233	1.10	4,233
0.08	308	0.60	2,271	1.12	4,273
0.00	346	0.61	2,348	1.12	4,312
0.10	385	0.62	2,340	1.13	4,389
0.11	423	0.63	2,425	1.15	4,007
0.12	462	0.64	2,464	1.16	4,466
0.13	500	0.65	2,502	1.17	4,504
0.14	539	0.66	2,541	1.18	4,543
0.15	577	0.67	2,579	1.19	4,581
0.16	616	0.68	2,618	1.20	4,620
0.17	654	0.69	2,656	1.20	4,658
0.18	693	0.70	2,695	1.22	4,697
0.19	731	0.71	2,733	1.22	4,735
0.20	770	0.72	2,772	1.24	4,774
0.21	808	0.73	2,810	1.25	4,812
0.22	847	0.74	2,849	1.26	4,812
0.23	885	0.75	2,887	1.20	4,889
0.24	924	0.76	2,926	1.28	4,928
0.25	962	0.77	2,964	1.29	4,966
0.26	1,001	0.78	3,003	1.30	5,005
0.27	1,039	0.79	3,041	1.31	5,043
0.28	1,078	0.80	3,080	1.32	5,082
0.29	1,116	0.81	3,118	1.33	5,120
0.30	1,155	0.82	3,157		•,•
0.31	1,193	0.83	3,195		
0.32	1,232	0.84	3,234		
0.33	1,270	0.85	3,272		
0.34	1,309	0.86	3,311		
0.35	1,347	0.87	3,349		
0.36	1,386	0.88	3,388		
0.37	1,424	0.89	3,426		
0.38	1,463	0.90	3,465		
0.39	1,501	0.91	3,503		
0.40	1,540	0.92	3,542		
0.41	1,578	0.93	3,580		
0.42	1,617	0.94	3,619		
0.43	1,655	0.95	3,657		
0.44	1,694	0.96	3,696		
0.45	1,732	0.97	3,734		
0.46	1,771	0.98	3,773		
0.47	1,809	0.99	3,811		
0.48	1,848	1.00	3,850		
0.49	1,886	1.01	3,888		
0.50	1,925	1.02	3,927		
0.51	1,963	1.03	3,965		

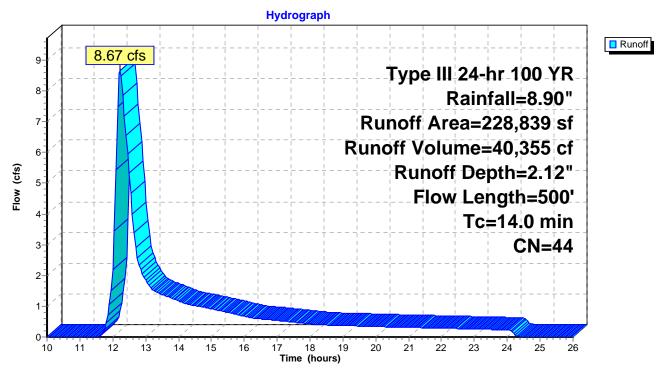
#### Time span=10.00-26.00 hrs, dt=0.05 hrs, 321 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Pre-Construction	Runoff Area=228,839 sf 9.80% Impervious Runoff Depth=2.12" Flow Length=500' Tc=14.0 min CN=44 Runoff=8.67 cfs 40,355 cf
Subcatchment 2S: Post-Construction F	Runoff Area=228,838 sf 14.00% Impervious Runoff Depth=2.46" Flow Length=500' Tc=14.0 min CN=47 Runoff=10.61 cfs 46,981 cf
Subcatchment 10S: DA#2 TO Pervious Pavem Flow Length=15	<b>ent</b> Runoff Area=64,365 sf 24.89% Impervious Runoff Depth=3.30" 0' Slope=0.0500 '/' Tc=9.4 min CN=54 Runoff=4.85 cfs 17,676 cf
Subcatchment 30S: Net Post-Construction	Runoff Area=164,473 sf 9.74% Impervious Runoff Depth=2.12"
	Flow Length=290' Tc=7.5 min CN=44 Runoff=7.60 cfs 29,004 cf
Pond 20P: Pervious Pavement Infiltration	Peak Elev=1.27' Storage=4,890 cf Inflow=4.85 cfs 17,676 cf
	Outflow=1.00 cfs 17,676 cf
	sf Runoff Volume = 134,017 cf Average Runoff Depth = 2.34" 87.40% Pervious = 600,015 sf 12.60% Impervious = 86,500 sf

			Summa	y IOI SUDC				
Runoff	=	8.67	cfs @ 12.	22 hrs, Volu	ume= 40,355 cf, Depth= 2.12"			
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.90"							
Type III 2	24-11/100	TR RUIN	iaii=0.90					
	Area (sf)	CN E	Description					
*	22,426	98 9	.8% Lot Co	overage				
	93,000	36 V	Voods, Fair	, HSG A				
	113,413	39 >	>75% Gras	s cover, Go	ood, HSG A			
	228,839	44 V	Veighted A	verage				
:	206,413	9	0.20% Per	vious Area				
	22,426	9	9.80% Impe	ervious Arec	1			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)		(Cfs)	becenpiion			
8.9	150	0.0570	/		Sheet Flow, Elev 122.5 to 114			
•					Grass: Short $n = 0.150$ P2= 3.20"			
5.1	350	0.0520	1.14		Shallow Concentrated Flow, To Cheswick Court			
					Woodland Kv= 5.0 fps			
14.0	500	Total						

Summary for Subcatchment 1S: Pre-Construction

#### Subcatchment 1S: Pre-Construction



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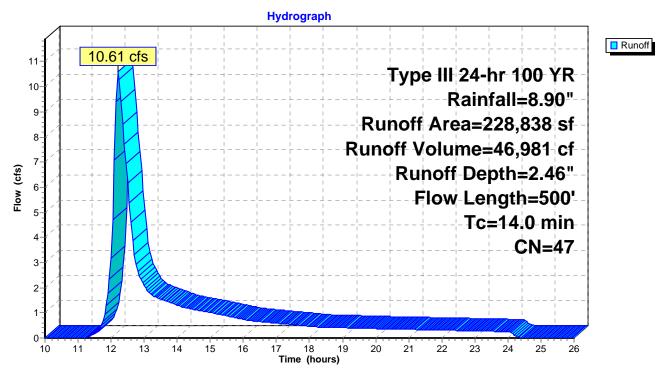
# Hydrograph for Subcatchment 1S: Pre-Construction

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)		(Cfs)		(inches)		(Cfs)
10.00	1.68	0.00	0.00	23.00	8.82	2.07	0.26
10.25	1.80	0.00	0.00	23.25	8.84	2.08	0.25
10.50	1.93	0.00	0.00	23.50	8.86	2.09	0.24
10.75	2.07	0.00	0.00	23.75	8.88	2.11	0.24
11.00	2.23	0.00	0.00	24.00	8.90	2.12	0.23
11.25	2.41	0.00	0.00	24.25	8.90	2.12	0.07
11.50	2.65	0.00	0.00	24.50	8.90	2.12	0.00
11.75	3.16	0.03	0.27	24.75	8.90	2.12	0.00
12.00	4.45	0.25	2.20	25.00	8.90	2.12	0.00
12.25	5.74	0.64	8.49	25.25	8.90	2.12	0.00
12.50	6.25	0.83	5.33	25.50	8.90	2.12	0.00
12.75 13.00	6.49 6.67	0.93 1.01	2.58 1.85	25.75 26.00	8.90 8.90	2.12 2.12	0.00 0.00
13.00	6.83	1.01	1.65	20.00	0.90	2.12	0.00
13.50	6.97	1.14	1.38				
13.75	7.10	1.20	1.28				
14.00	7.22	1.25	1.17				
14.25	7.32	1.30	1.07				
14.50	7.42	1.35	1.02				
14.75	7.52	1.40	0.97				
15.00	7.60	1.44	0.91				
15.25	7.68	1.48	0.85				
15.50	7.76	1.51	0.80				
15.75	7.82	1.55	0.73				
16.00	7.89	1.58	0.67				
16.25	7.94	1.61	0.62				
16.50	8.00	1.63	0.59				
16.75	8.05	1.66	0.56				
17.00 17.25	8.09 8.14	1.68	0.53 0.51				
17.25	8.18	1.71 1.73	0.51				
17.75	8.22	1.75	0.40				
18.00	8.26	1.77	0.42				
18.25	8.29	1.79	0.40				
18.50	8.33	1.81	0.39				
18.75	8.36	1.82	0.38				
19.00	8.39	1.84	0.37				
19.25	8.43	1.86	0.36				
19.50	8.46	1.88	0.35				
19.75	8.49	1.89	0.34				
20.00	8.52	1.91	0.34				
20.25	8.55	1.92	0.33				
20.50	8.57	1.94	0.32				
20.75 21.00	8.60 8.63	1.95 1.97	0.32 0.31				
21.00	8.65	1.97	0.30				
21.20	8.68	1.99	0.30				
21.00	8.70	2.01	0.29				
22.00	8.73	2.02	0.28				
22.25	8.75	2.03	0.28				
22.50	8.78	2.05	0.27				
22.75	8.80	2.06	0.26				
				•			

	Summary for Subcatchment 2S: Post-Construction								
Runoff	=	10.61 c	fs @ 12.	22 hrs, Volu	ume= 46,981 cf, Depth= 2.46"				
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.90"								
ŀ	Area (sf)	CN D	escription						
*	32,037	98 14	4% Lot Co	verage					
	24,000	36 W	'oods, Fair	r, HSG A					
1	72,801	39 >	75% Gras	s cover, Go	ood, HSG A				
2	28,838	47 W	eighted A	verage					
1	96,801	80	5.00% Per	vious Area					
	32,037	14	4.00% Imp	pervious Are	a				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.9	150	0.0570	0.28		Sheet Flow, Elev 122.5 to 114				
					Grass: Short n= 0.150 P2= 3.20"				
5.1	350	0.0520	1.14		Shallow Concentrated Flow, To Cheswick Court				
					Woodland Kv= 5.0 fps				

14.0 500 Total

#### Subcatchment 2S: Post-Construction



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# Hydrograph for Subcatchment 2S: Post-Construction

Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(Cfs)	(hours)	(inches)	(inches)	(Cfs)
10.00	1.68	0.00	0.00	23.00	8.82	2.42	0.28
10.25	1.80	0.00	0.00	23.25	8.84	2.43	0.27
10.50	1.93	0.00	0.00	23.50	8.86	2.44	0.26
10.75	2.07	0.00	0.00	23.75	8.88	2.45	0.26
11.00	2.23	0.00	0.00	24.00	8.90	2.46	0.25
11.25	2.41	0.00	0.02	24.25	8.90	2.46	0.07
11.50	2.65	0.01	0.16	24.50	8.90	2.46	0.01
11.75	3.16	0.07	0.67	24.75	8.90	2.46	0.00
12.00	4.45	0.36	3.17	25.00	8.90	2.46	0.00
12.25	5.74	0.82	10.29	25.25	8.90	2.46	0.00
12.50	6.25	1.04	6.17	25.50	8.90	2.46	0.00
12.75	6.49	1.15	2.93	25.75	8.90	2.46	0.00
13.00	6.67	1.24	2.09	26.00	8.90	2.46	0.00
13.25 13.50	6.83 6.97	1.32 1.39	1.69 1.55				
13.50	7.10	1.39	1.55				
14.00	7.22	1.40	1.45				
14.25	7.32	1.57	1.20				
14.50	7.42	1.62	1.13				
14.75	7.52	1.67	1.07				
15.00	7.60	1.72	1.01				
15.25	7.68	1.76	0.95				
15.50	7.76	1.80	0.88				
15.75	7.82	1.84	0.81				
16.00	7.89	1.87	0.74				
16.25	7.94	1.91	0.68				
16.50	8.00	1.94	0.65				
16.75	8.05	1.96	0.62				
17.00	8.09	1.99	0.59				
17.25	8.14	2.02	0.56				
17.50 17.75	8.18 8.22	2.04 2.06	0.52 0.49				
17.75	8.22 8.26	2.08	0.49				
18.25	8.29	2.07	0.43				
18.50	8.33	2.13	0.40				
18.75	8.36	2.15	0.41				
19.00	8.39	2.16	0.40				
19.25	8.43	2.18	0.40				
19.50	8.46	2.20	0.39				
19.75	8.49	2.22	0.38				
20.00	8.52	2.24	0.37				
20.25	8.55	2.25	0.36				
20.50	8.57	2.27	0.35				
20.75	8.60	2.29	0.34				
21.00	8.63	2.30	0.34				
21.25 21.50	8.65 8.68	2.32 2.33	0.33 0.32				
21.50	0.00 8.70	2.33	0.32				
21.75	8.73	2.35	0.32				
22.00	8.75	2.30	0.30				
22.50	8.78	2.39	0.29				
22.75	8.80	2.40	0.29				
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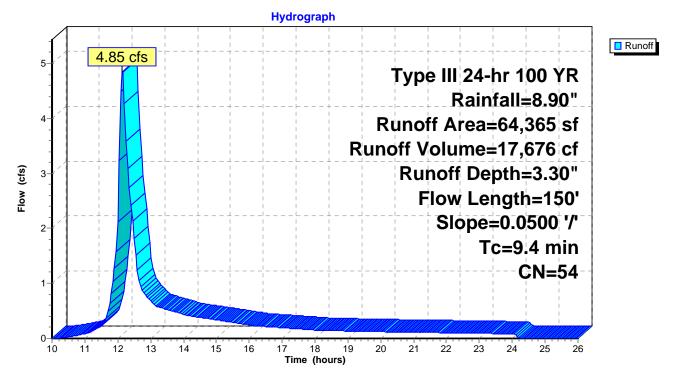
#### Summary for Subcatchment 10S: DA#2 TO Pervious Pavement Section

Runoff = 4.85 cfs @ 12.14 hrs, Volume = 17,676 cf, Depth = 3.30"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.90"

	A	Area (sf)	CN	Description		
*		16,022	98			
		48,343	39	>75% Gras	s cover, Go	ood, HSG A
		64,365	54	Weighted A	verage	
		48,343		75.11% Per	vious Area	
		16,022		24.89% Imp	pervious Are	a
	Tc	Length	Slop	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/f	t) (ft/sec)	(Cfs)	
	9.4	150	0.050	0 0.27		Sheet Flow, ELEV. 122.5 TO 115
						Grass: Short n= 0.150 P2= 3.20"

#### Subcatchment 10S: DA#2 TO Pervious Pavement Section



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# Hydrograph for Subcatchment 10S: DA#2 TO Pervious Pavement Section

		_				_	
Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(Cfs)	(hours)	(inches)	(inches)	(cfs)
10.00	1.68	0.00	0.00	23.00	8.82	3.24	0.09
10.25	1.80	0.00	0.00	23.25	8.84	3.25	0.09
10.50	1.93	0.01	0.03	23.50	8.86	3.27	0.09
10.75	2.07	0.02	0.05	23.75	8.88	3.28	0.08
11.00	2.23	0.03	0.09	24.00	8.90	3.30	0.08
11.25	2.41	0.05	0.14	24.25	8.90	3.30	0.01
11.50	2.65	0.10	0.23	24.50	8.90	3.30	0.00
11.75	3.16	0.21	0.64	24.75	8.90	3.30	0.00
12.00	4.45	0.67	2.12	25.00	8.90	3.30	0.00
12.25	5.74	1.30	3.58	25.25	8.90	3.30	0.00
12.20	6.25	1.58	1.82	25.50	8.90	3.30	0.00
12.30	6.49	1.30	0.87	25.75	8.90	3.30	0.00
13.00	6.67	1.83	0.68	26.00	8.90	3.30	0.00
13.25	6.83	1.93	0.57				
13.50	6.97	2.01	0.52				
13.75	7.10	2.09	0.48				
14.00	7.22	2.17	0.44				
14.25	7.32	2.23	0.40				
14.50	7.42	2.30	0.38				
14.75	7.52	2.36	0.36				
15.00	7.60	2.41	0.34				
15.25	7.68	2.47	0.31				
15.50	7.76	2.51	0.29				
15.75	7.82	2.56	0.27				
16.00	7.89	2.60	0.24				
16.25	7.94	2.64	0.23				
16.50	8.00	2.67	0.21				
16.75	8.05	2.71	0.20				
17.00	8.09	2.74	0.19				
17.25	8.14	2.77	0.18				
17.50	8.18	2.80	0.17				
17.75	8.22	2.83	0.16				
18.00	8.26	2.85	0.15				
18.25	8.29	2.87	0.14				
18.50	8.33	2.90	0.14				
18.75	8.36	2.92	0.14				
19.00	8.39	2.94	0.13				
19.25	8.43	2.97	0.13				
19.50	8.46	2.99	0.13				
19.75	8.49	3.01	0.12				
20.00	8.52	3.03	0.12				
20.00	8.55	3.05	0.12				
20.23	8.57	3.03	0.12				
20.75 21.00	8.60 8.63	3.09	0.11 0.11				
		3.10					
21.25	8.65	3.12	0.11				
21.50	8.68	3.14	0.11				
21.75	8.70	3.16	0.10				
22.00	8.73	3.17	0.10				
22.25	8.75	3.19	0.10				
22.50	8.78	3.21	0.10				
22.75	8.80	3.22	0.09				

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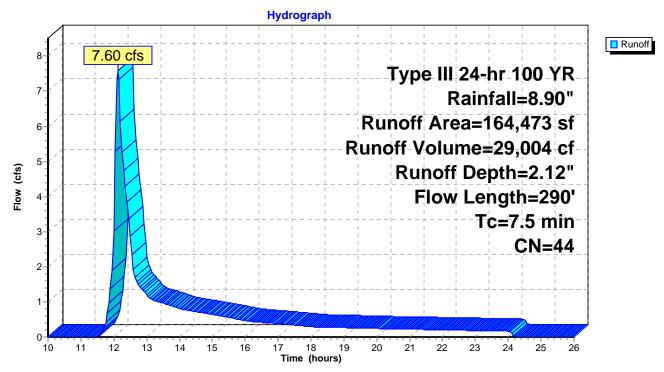
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		Su	immary fo	or Subcate	chment 30S: Net Post-Construction
Runoff	=	7.60	cfs @ 12.	12 hrs, Volu	ume= 29,004 cf, Depth= 2.12"
	•		od, UH=SC fall=8.90"	CS, Time Spo	an= 10.00-26.00 hrs, dt= 0.05 hrs
	Area (sf)	CN E	Description		
*	16,015	98 1	4% Lot Co	verage less	s pavement
	24,000	36 V	Voods, Fair	, HSG A	
1	24,458	39 >	>75% Gras	s cover, Go	bod, HSG A
	64,473	44 V	Veighted A	verage	
Ī	48,458	9	0.26% Per	vious Area	
	16,015	9	9.74% Impe	ervious Arec	1
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	-	(cfs)	
4.8	66	0.0530	0.23		Sheet Flow, Elev 116 to 112.5
					Grass: Short n= 0.150 P2= 3.20"
2.7	224	0.0750	1.37		Shallow Concentrated Flow, To Cheswick Court
					Woodland Kv= 5.0 fps
7.5	290	Total			

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### Subcatchment 30S: Net Post-Construction



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# Hydrograph for Subcatchment 30S: Net Post-Construction

		_				_	
Time	Precip.	Excess	Runoff	Time	Precip.	Excess	Runoff
(hours)	(inches)	(inches)	(Cfs)	(hours)	(inches)	(inches)	(cfs)
10.00	1.68	0.00	0.00	23.00	8.82	2.07	0.18
10.25	1.80	0.00	0.00	23.25	8.84	2.08	0.18
10.50	1.93	0.00	0.00	23.50	8.86	2.09	0.17
10.75	2.07	0.00	0.00	23.75	8.88	2.11	0.17
11.00	2.23	0.00	0.00	24.00	8.90	2.12	0.16
11.25	2.41	0.00	0.00	24.25	8.90	2.12	0.00
11.50	2.65	0.00	0.01	24.50	8.90	2.12	0.00
11.75	3.16	0.03	0.43	24.75	8.90	2.12	0.00
12.00	4.45	0.25	3.02	25.00	8.90	2.12	0.00
12.00	5.74	0.64	5.27	25.25	8.90	2.12	0.00
12.20	6.25	0.83	2.87	25.50	8.90	2.12	0.00
12.30	6.49	0.93	1.49	25.75	8.90	2.12	0.00
13.00	6.67	1.01	1.20	26.00	8.90	2.12	0.00
13.25	6.83	1.08	1.03				
13.50	6.97	1.14	0.96				
13.75	7.10	1.20	0.89				
14.00	7.22	1.25	0.81				
14.25	7.32	1.30	0.75				
14.50	7.42	1.35	0.72				
14.75	7.52	1.40	0.68				
15.00	7.60	1.44	0.64				
15.25	7.68	1.48	0.60				
15.50	7.76	1.51	0.55				
15.75	7.82	1.55	0.51				
16.00	7.89	1.58	0.47				
16.25	7.94	1.61	0.43				
16.50	8.00	1.63	0.41				
16.75	8.05	1.66	0.40				
17.00	8.09	1.68	0.38				
17.25	8.14	1.71	0.36				
17.50	8.18	1.73	0.34				
17.75	8.22	1.75	0.31				
18.00	8.26	1.77	0.29				
18.25	8.29	1.79	0.28				
18.50	8.33	1.81	0.28				
18.75	8.36	1.82	0.27				
19.00	8.39	1.84	0.26				
19.25	8.43	1.86	0.26				
19.50	8.46	1.88	0.25				
19.75	8.49	1.89	0.25				
20.00	8.52	1.91	0.24				
20.25	8.55	1.92	0.24				
20.20	8.57	1.94	0.23				
20.75	8.60	1.95	0.20				
21.00	8.63	1.97	0.22				
21.00	8.65	1.97	0.22				
21.25	8.68	1.90	0.22				
21.50	8.70	2.01	0.21				
22.00	8.73	2.02	0.20				
22.25	8.75	2.03	0.20				
22.50	8.78	2.05	0.19				
22.75	8.80	2.06	0.19	l			

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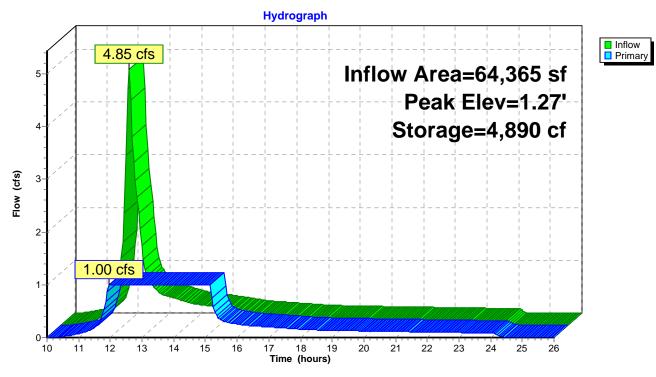
# Summary for Pond 20P: Pervious Pavement Infiltration

Inflow Ar Inflow Outflow Primary	=	4.85 cfs @ 1 1.00 cfs @ 1	24.89% Impervious, Inflow Depth = 3.30" for 100 YR event         2.14 hrs, Volume = 17,676 cf         1.95 hrs, Volume = 17,676 cf, Atten = 79%, Lag = 0.0 min         1.95 hrs, Volume = 17,676 cf			
Routing by Stor-Ind method, Time Span= 10.00-26.00 hrs, dt= 0.05 hrs Peak Elev= 1.27' @ 12.67 hrs Surf.Area= 0 sf Storage= 4,890 cf						
Plug-Flow detention time= 35.4 min calculated for 17,621 cf (100% of inflow) Center-of-Mass det. time= 35.3 min ( 892.2 - 857.0 )						
Volume	Invert	Avail.Sto	age Storage Description			
#1	0.00	5,12	20 cf Custom Stage Data Listed below			
Elevatio (fee 0.0 1.3	et) (cuk )0	m.Store <u>bic-feet)</u> 0 5,120				
Device	Routing	Invert	Outlet Devices			
#1	Primary	0.00'	<b>9600 sq. ff. INFILTRATION</b> Elev. (feet) 0.00 0.10 1.00 Disch. (cfs) 0.000 1.000 1.000			

Primary OutFlow Max=1.00 cfs @ 11.95 hrs HW=0.11' (Free Discharge)

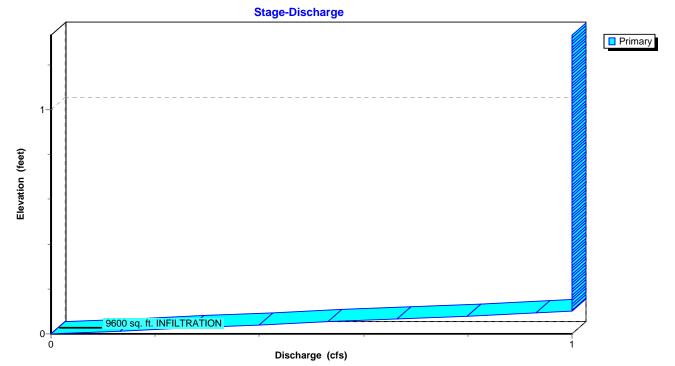
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Performance Stage-Area-Storage

#### Pond 20P: Pervious Pavement Infiltration

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# Hydrograph for Pond 20P: Pervious Pavement Infiltration

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
10.00	0.00	0	0.00	0.00
10.50	0.03	7	0.00	0.02
11.00	0.09	28	0.01	0.07
11.50	0.23	74	0.02	0.19
12.00	2.12	573	0.15	1.00
12.50	1.82	4,673	1.21	1.00
13.00	0.68	4,661	1.21	1.00
13.50	0.52	3,904	1.01	1.00
14.00	0.44	2,971	0.77	1.00
14.50	0.38	1,899	0.49	1.00
15.00	0.34	745	0.19	1.00
15.50	0.29	125	0.03	0.32
16.00	0.24	98	0.03	0.25
16.50	0.21	84	0.02	0.22
17.00	0.19	76	0.02	0.20
17.50	0.17	68	0.02	0.18
18.00	0.15	60	0.02	0.16
18.50	0.14	54	0.01	0.14
19.00	0.13	52	0.01	0.14
19.50	0.13	50	0.01	0.13
20.00	0.12	47	0.01	0.12
20.50	0.12	45	0.01	0.12
21.00	0.11	43	0.01	0.11
21.50	0.11	41	0.01	0.11
22.00	0.10	39	0.01	0.10
22.50	0.10	37	0.01	0.10
23.00	0.09	36	0.01	0.09
23.50	0.09	34	0.01	0.09
24.00	0.08	32	0.01	0.08
24.50	0.00	1	0.00	0.00
25.00	0.00	0	0.00	0.00
25.50	0.00	0	0.00	0.00
26.00	0.00	0	0.00	0.00

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# Stage-Discharge for Pond 20P: Pervious Pavement Infiltration

Elevation	Primary	Elevation	Primary	Elevation	Primary
(feet)	(cfs)	(feet)	(cfs)	(feet)	(cfs)
0.00	0.00	0.52	1.00	1.04	1.00
0.01	0.10	0.53	1.00	1.05	1.00
0.02	0.20	0.54	1.00	1.06	1.00
0.03	0.30	0.55	1.00	1.07	1.00
0.04	0.40	0.56	1.00	1.08	1.00
0.05	0.50	0.57	1.00	1.09	1.00
0.06	0.60	0.58	1.00	1.10	1.00
0.07	0.70	0.59	1.00	1.11	1.00
0.08	0.80	0.60	1.00	1.12	1.00
0.09	0.90	0.61	1.00	1.13	1.00
0.10	1.00	0.62	1.00	1.14	1.00
0.11	1.00	0.63	1.00	1.15	1.00
0.12	1.00	0.64	1.00	1.16	1.00
0.13	1.00	0.65	1.00	1.17	1.00
0.14	1.00	0.66	1.00	1.18	1.00
0.15	1.00	0.67	1.00	1.19	1.00
0.16	1.00	0.68	1.00	1.20	1.00
0.17	1.00	0.69	1.00	1.21	1.00
0.18	1.00	0.70	1.00	1.22	1.00
0.19 0.20	1.00 1.00	0.71 0.72	1.00 1.00	1.23	1.00 1.00
0.20	1.00	0.72	1.00	1.24 1.25	1.00
0.21	1.00	0.73	1.00	1.25	1.00
0.22	1.00	0.74	1.00	1.20	1.00
0.24	1.00	0.76	1.00	1.27	1.00
0.25	1.00	0.77	1.00	1.29	1.00
0.26	1.00	0.78	1.00	1.30	1.00
0.27	1.00	0.79	1.00	1.31	1.00
0.28	1.00	0.80	1.00	1.32	1.00
0.29	1.00	0.81	1.00	1.33	1.00
0.30	1.00	0.82	1.00		
0.31	1.00	0.83	1.00		
0.32	1.00	0.84	1.00		
0.33	1.00	0.85	1.00		
0.34	1.00	0.86	1.00		
0.35	1.00	0.87	1.00		
0.36	1.00	0.88	1.00		
0.37	1.00	0.89	1.00		
0.38	1.00	0.90	1.00		
0.39	1.00	0.91	1.00		
0.40	1.00	0.92	1.00		
0.41	1.00	0.93	1.00		
0.42	1.00	0.94	1.00		
0.43	1.00	0.95	1.00		
0.44	1.00	0.96	1.00		
0.45	1.00	0.97	1.00		
0.46	1.00	0.98	1.00		
0.47 0.48	1.00 1.00	0.99 1.00	1.00 1.00		
0.48	1.00	1.00	1.00		
0.49	1.00	1.01	1.00		
0.50	1.00	1.02	1.00		
0.01	1.00	1.00	1.00	I	

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# Stage-Area-Storage for Pond 20P: Pervious Pavement Infiltration

Elevation	Storage	Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)	(feet)	(cubic-feet)
0.00	0	0.52	2,002	1.04	4,004
0.01	38	0.53	2,040	1.05	4,042
0.02	77	0.54	2,079	1.06	4,081
0.03	115	0.55	2,117	1.07	4,119
0.04	154	0.56	2,156	1.08	4,158
0.05	194	0.57	2,194	1.00	4,196
0.06	231	0.58	2,174	1.10	4,170
0.07	269	0.59	2,233	1.10	4,233
0.08	308	0.60	2,271	1.12	4,273
0.00	346	0.61	2,348	1.12	4,312
0.10	385	0.62	2,340	1.13	4,389
0.11	423	0.63	2,425	1.15	4,007
0.12	462	0.64	2,423	1.16	4,427
0.13	500	0.65	2,502	1.17	4,504
0.14	539	0.66	2,541	1.18	4,543
0.15	577	0.67	2,579	1.10	4,543
0.16	616	0.68	2,618	1.19	4,620
0.17	654	0.69	2,656	1.20	4,658
0.18	693	0.70	2,695	1.22	4,697
0.19	731	0.70	2,073	1.22	4,097
0.19	770	0.72	2,733	1.23	4,733
0.20	808	0.72	2,810	1.24	4,774
0.22	847	0.74	2,849	1.26	4,812
0.22	885	0.75	2,847	1.20	4,889
0.23	924	0.76	2,007	1.27	4,007
0.24	962	0.77	2,920	1.20	4,920
0.26	1,001	0.78	3,003	1.30	5,005
0.20	1,039	0.79	3,003	1.30	5,003
0.28	1,078	0.80	3,080	1.31	5,082
0.29	1,116	0.81	3,118	1.33	5,120
0.30	1,155	0.82	3,157	1.55	5,120
0.31	1,193	0.83	3,195		
0.32	1,173	0.84	3,234		
0.33	1,202	0.85	3,272		
0.34	1,309	0.86	3,311		
0.35	1,347	0.87	3,349		
0.36	1,386	0.88	3,388		
0.37	1,424	0.89	3,426		
0.38	1,463	0.90	3,465		
0.39	1,501	0.91	3,503		
0.40	1,540	0.92	3,542		
0.41	1,578	0.93	3,580		
0.42	1,617	0.94	3,619		
0.43	1,655	0.95	3,657		
0.44	1,694	0.96	3,696		
0.45	1,732	0.97	3,734		
0.46	1,771	0.98	3,773		
0.47	1,809	0.99	3,811		
0.48	1,848	1.00	3,850		
0.49	1,886	1.01	3,888		
0.50	1,925	1.02	3,927		
0.51	1,963	1.03	3,965		
				•	

# E| Drainage Area Map

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